

DEPARTMENT OF ENERGETICS



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Consistency of Multiple-relaxation-time Lattice Boltzmann Schemes for Mixture Modeling

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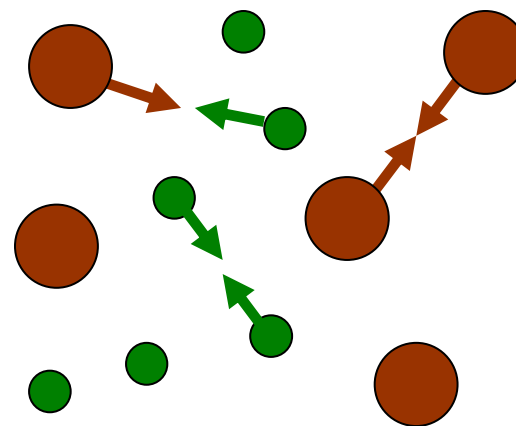
Invited Talk (Prof. Taku Ohwada)

**Department of Aeronautics and
Astronautics**

Graduate School of Engineering

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Politecnico di Torino

The Politecnico has **26,000 students**, 890 lecturers and researchers, and around 800 administration staff. There are **6 Schools**, **1 Graduate School**, 18 Departments and 7 Interdepartmental Centres. The income in the 2005 balance was **223 million Euros** (53 % from the State).



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Outline

- (1) Simplified **Kinetic Model Equations** for Multi–species Single–phase Mixtures
- (2) Numerical **LBM Scheme** and Practical Details
- (3) **Diffusion Process** at Macroscopic Level
- (4) **Semi–implicit** Discretization Strategies
- (5) Application:
 - **Direct Numerical Simulation** (DNS) of Decaying Homogenous Isotropic Turbulence (DHIT)



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Simplified Kinetic Model Equations for Multi-species Single-phase Mixtures



Preliminary Snapshot

- There is considerably **more latitude** in the choice of a **linearization procedure** in the case of a mixture than for a pure gas (Stewart Harris, 1971)...



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$$Df_{\sigma}/Dt = Q_{\sigma\sigma} + Q_{\sigma m} = Q_{\sigma\sigma} + \sum_{\zeta} Q_{\sigma\zeta}$$

$$Df_{\sigma}/Dt = 0 + \lambda_n^{\sigma} (f_n^e - f_{\sigma})$$

$$Df_{\sigma}/Dt = 0 + \lambda_m (f_m^e - f_{\sigma})$$

$$Df_{\sigma}/Dt = \lambda_{\sigma} (f_{\sigma}^e - f_{\sigma}) + \lambda_m f_{\sigma}^e / e_{\sigma} (\mathbf{v} - \mathbf{u}_{\sigma}) \cdot \mathbf{w}_{\sigma}$$

$$Df_{\sigma}/Dt = \lambda_{\sigma} (f_{\sigma}^e - f_{\sigma}) + \lambda_m (f_m^e - f_{\sigma})$$



Possible Linearizations

- In particular considering the target **macroscopic velocity** (only **athermal LB models** will be discussed here), some reasonable linearizations are...



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$$f_*^e = f^e(\mathbf{u}_*, e_*) = \frac{\rho_\sigma}{m_\sigma (2\pi e_*)^{D/2}} \exp \left[-\frac{(\mathbf{v} - \mathbf{u}_*)^2}{2 e_*} \right]$$

$$f_n^e = f^e(\mathbf{u}_n, e_\sigma) \leftarrow \mathbf{u}_n = \frac{\sum_\sigma m_\sigma \mathbf{u}_\sigma}{\sum_\sigma m_\sigma}$$

$$f_m^e = f^e(\mathbf{u}, e_\sigma) \leftarrow \mathbf{u} = \frac{\sum_\sigma \rho_\sigma \mathbf{u}_\sigma}{\sum_\sigma \rho_\sigma}$$

$$f_\sigma^e = f^e(\mathbf{u}_\sigma, e_\sigma) \leftarrow \mathbf{u}_\sigma$$



(1) Gross & Krook Model

- **Single – Fluid Approach:** the total effects due to both self and cross collisions are modeled by a BGK–like operator involving a Maxwellian centered on **the mass weighted velocity** (selected for ensuring the same momentum relaxation equation due to the full Boltzmann equations, i.e. Morse’s procedure)
- Lattice Boltzmann version has been proposed (Shan & Chen, PRE 1993; Shan & Doolen, JSP 1995)



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$$\frac{Df_{\sigma}}{Dt} = \lambda_n^{\sigma} [f_n^e(\mathbf{u}_n) - f_{\sigma}] \leftarrow \mathbf{u}_n = \frac{\sum_{\sigma} m_{\sigma} \mathbf{u}_{\sigma}}{\sum_{\sigma} m_{\sigma}}$$



Gross & Krook Model: (Some) Limits

- The relaxation frequencies must be selected for ensuring the **macroscopic barycentric momentum conservation for the mixture**

$$\sum_{\sigma} \lambda_n^{\sigma} \rho_{\sigma} (\mathbf{u}_n - \mathbf{u}_{\sigma}) = 0 \rightarrow \lambda_n^{\sigma} = km_{\sigma} / \rho_{\sigma}$$

- From the macroscopic point of view, the kinematic viscosity of each species, the mutual diffusivity and the mixture kinematic viscosity are **coupled to each other**
- Models consistent with this approach usually involve an **interaction pseudo-potential** or a **long-range coupling force** for recovering the desired diffusion equations by an additional momentum exchange among particles





Consistency for BGK-Type Models

- **Basic consistency constraints** (Aoki *et al.*, JSP 2002) in the design of simplified kinetic models for mixture modeling (LB model):
 1. the “Indifferentiability Principle” holds (??);
 2. the same relaxation equations for momentum and temperature derived by means of the full Boltzmann equations hold (~OK);
 3. the equilibrium distributions are Maxwellians with common velocities and internal energies (~OK);
 4. the non-negativity of densities is satisfied (NO);
 5. the H theorem holds (NO).



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Indifferentiability Principle

- The **Indifferentiability Principle** (dos Santos *et al.*, Phys. Fluids A 1989) prescribes that, if a BGK-like equation for each species is assumed, this set of equations should reduce to a **single BGK-like equation, when mechanically identical components are considered** (microscopic formulation, μ IP)
- This essentially means that, when all the species are identical, one should recover at macroscopic levels the equations governing the **single component gas dynamics** (macroscopic formulation, MIP)
- This property is satisfied by the bilinearity of the collision operator in the **full Boltzmann equations**



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Gross & Krook Model Does Not Satisfy μ IP

- Even though all the masses are identical, i.e.



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$$m_\sigma = m \rightarrow \mathbf{u}_n = \sum_{\sigma} \mathbf{u}_\sigma / N$$

$$\frac{Df}{Dt} = \sum_{\sigma} \lambda_n^\sigma [f_n^e(\mathbf{u}_n) - f_\sigma] \leftarrow \lambda_n^\sigma = km / \rho_\sigma$$

the total distribution does not satisfy a single BGK-like equation \rightarrow the Gross & Krook Model does not satisfy the Indifferentiability Principle (the previous proof refers to the microscopic formulation μ IP)



(2) Corrected Gross & Krook Model

- For satisfying the Indifferentiability Principle is enough to consider the **barycentric (density weighted) velocity** in the target Maxwellian (Lattice Boltzmann version by Sofonea & Sekerka, Physica A 2001)

$$\frac{Df_\sigma}{Dt} = \lambda_m [f_m^e(\mathbf{u}) - f_\sigma] \leftarrow \mathbf{u} = \frac{\sum_\sigma \rho_\sigma \mathbf{u}_\sigma}{\sum_\sigma \rho_\sigma}$$

- Selecting the same relaxation frequency ensures the **macroscopic barycentric momentum conservation for the mixture**, as well as that the **Indifferentiability Principle** holds, when all the same masses are considered (self evident !)





Corrected G&K Model : Peculiarities

$$\lambda_m \rightarrow \nu(\lambda_m), D(\lambda_m)$$

- Since both transport coefficients depend on the only relaxation frequency, the model implies a **fixed Schmidt number** ($Sc = \nu/D$)
- The momentum relaxation equation derived by the model is not the same obtained by the full Boltzmann equations, i.e. **Morse condition does not apply**: are we really increasing the consistency of the model ?
- As it will be showed later on, as far as **the macroscopic description is the main concern** (as it happens usually for LB schemes) and **only one property can be satisfied**, the Indifferentiability Principle must be preferred





(3) Sirovich Model

- **Multi – Fluid Approach with Force Coupling**: each species evolves according to the specific properties → a proper coupling must be introduced for modeling the diffusivity → theoretical background given by Sirovich model for $\beta=0$ → Luo & Girimaji, PRE 2003 (~) and A. Xu, Europhys. Letters 2005

$$\frac{Df_\sigma}{Dt} = \lambda_\sigma [f_\sigma^e(\mathbf{u}_\sigma) - f_\sigma] + \lambda_m \mathbf{c}_\sigma \cdot \mathbf{w}_\sigma \leftarrow \mathbf{w}_\sigma = \mathbf{u}_\sigma - \mathbf{u}$$

$$\mathbf{c}_\sigma = [f_\sigma^e(\mathbf{u}_\sigma) (1 - \beta) (\mathbf{v} - \mathbf{u}_\sigma) - f_m^e(\mathbf{u}) \beta (\mathbf{v} - \mathbf{u})] / e_\sigma$$

- Actually selecting $\beta=1/2$ (**central difference approximation**) ensures the maximum accuracy with regards to the original bilinear operator





Sirovich Model: Limits



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$$\lambda_\sigma, \lambda_m \rightarrow \nu = \frac{\sum_\sigma \rho_\sigma \nu_\sigma(\lambda_\sigma)}{\sum_\sigma \rho_\sigma}, \quad D(\lambda_m)$$

- Mixture viscosity is **decoupled** by the diffusion transport coefficient \rightarrow (moderately) tunable Schmidt number \rightarrow for modeling large Schmidt number (i.e. phenomena ruled by small diffusion) a **large forcing term** is needed.
- The Sirovich model **does not satisfy the Indifferentiability Principle** (even for $\beta=1$)

$$\frac{Df}{Dt} = \sum_\sigma \lambda_\sigma [f_\sigma^e(\mathbf{u}_\sigma) - f_\sigma] + \lambda_m (1 - \beta) \sum_\sigma f_\sigma^e(\mathbf{u}_\sigma) / e(\mathbf{v} - \mathbf{u}_\sigma)$$



(4) Hamel Model

- **Complete Multi – Fluid Approach:** cross collisions are described by an independent BGK–like collisional operator (similar to self collisions) → theoretical background given by Hamel model (Asinari, POF 2005).

$$\frac{Df_{\sigma}}{Dt} = \lambda_{\sigma} [f_{\sigma}^e(\mathbf{u}_{\sigma}) - f_{\sigma}] + \lambda_m [f_m^e(\mathbf{u}) - f_{\sigma}]$$

- Improved modeling of cross collisions which **effect both the mixture viscosity and the diffusivity** (as they actually do in reality !)
- The Hamel model **does not satisfy the Indifferentiability Principle** (analogously to the Sirovich model for $\beta=1$)





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Numerical LBM Scheme and Practical Details



SRT vs. MRT

- Single-relaxation-time (SRT) formulation **limits**:
 - tuning lattice energy levels can lead the **algorithm to diverge** for large mass ratios;
 - relaxation time constant for cross collisions must be tuned in order to recover **EITHER the diffusivity OR the mixture viscosity**.
- Multiple-relaxation-time (MRT) formulation **patches**:
 - over-relaxing the non-conserved modes, without affecting the main transport coefficients, **can partially avoid instability**;
 - relaxing differently the cross collisional modes can **decouple** diffusivity and mixture viscosity.



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MRT Hamel Model

- Introducing a **proper lattice** with Q components...

$$f_\sigma \rightarrow \mathbf{f}_\sigma \in \mathbb{R}^Q$$

$$\frac{D\mathbf{f}_\sigma}{Dt} = \mathbf{A}_\sigma [\mathbf{f}_\sigma^e(\mathbf{u}_\sigma) - \mathbf{f}_\sigma] + \mathbf{A}_m [\mathbf{f}_m^e(\mathbf{u}) - \mathbf{f}_\sigma]$$

$$\mathbf{A}_\sigma = \mathbf{M}_D^{-1} \mathbf{D}_\sigma \mathbf{M}_D, \quad \mathbf{A}_m = \mathbf{M}_D^{-1} \mathbf{D}_m \mathbf{M}_D$$

$$\text{diag}(\mathbf{D}_\sigma) = [0, 0, 0, \lambda_{\sigma\nu}^{II}, \lambda_{\sigma\nu}^{II}, \lambda_{\sigma\eta}^{II}, \lambda_\sigma^{III}, \lambda_\sigma^{III}, \lambda_\sigma^{IV}]^T$$

$$\text{diag}(\mathbf{D}_m) = [0, \lambda_m^I, \lambda_m^I, \lambda_{m\nu}^{II}, \lambda_{m\nu}^{II}, \lambda_{m\eta}^{II}, \lambda_m^{III}, \lambda_m^{III}, \lambda_m^{IV}]^T$$

- This implies a **large set of additional degrees of freedom** which can be tuned in the model for improving the reliability at macroscopic level with regards to the transport coefficients



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Compact MRT Hamel Model

- Since all the collision terms in the MRT Hamel model are **linear** with regards to the probability distribution functions, it is possible to rewrite this model for showing that it essentially implies a **different equilibrium function**

$$\frac{\partial \mathbf{f}_\sigma}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{f}_\sigma = \mathbf{A}_* (\mathbf{f}_*^e - \mathbf{f}_\sigma)$$

$$\mathbf{f}_*^e = (\mathbf{I} - \mathbf{M}_D^{-1} \mathbf{X}_\sigma^0 \mathbf{M}_D) \mathbf{f}_\sigma^e + \mathbf{M}_D^{-1} \mathbf{X}_\sigma^0 \mathbf{M}_D \mathbf{f}_m^e$$

- Far from the **Boltzmann equations** for mixtures !!

$$Q_{\sigma\sigma} + \sum_{\zeta} Q_{\sigma\zeta} = 0 \rightarrow f_\sigma = f_m^e$$

$$\mathbf{A}_* (\mathbf{f}_*^e - \mathbf{f}_\sigma) = 0 \rightarrow \mathbf{f}_\sigma = \mathbf{f}_*^e \quad (?!)$$



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Asymptotic Analysis

- Applying the **diffusive scaling**, the macroscopic equations can be recovered by means of the asymptotic analysis for LBM (Junk et al., JCP 2005)

$$\begin{aligned}
 \frac{\partial}{\partial \hat{t}} (\hat{\rho}_\sigma \hat{\mathbf{u}}_\sigma) &+ \hat{\nabla} \cdot \left[(1 - \alpha_{\sigma\nu}^{II}) \hat{\rho}_\sigma \hat{\mathbf{u}}_\sigma \otimes \hat{\mathbf{u}}_\sigma + \alpha_{\sigma\nu}^{II} \hat{\rho}_\sigma \hat{\mathbf{u}} \otimes \hat{\mathbf{u}} \right] \\
 &= -\hat{\nabla} \hat{p}_\sigma + \hat{\nabla} \left[\hat{\eta}_{\sigma m} \hat{\nabla} \cdot (\hat{\rho}_\sigma \hat{\mathbf{u}}_\sigma) \right] \\
 &+ \hat{\nabla} \cdot \left[\hat{\nu}_{\sigma m} \hat{\nabla} (\hat{\rho}_\sigma \hat{\mathbf{u}}_\sigma) + \hat{\nu}_{\sigma m} \hat{\nabla} (\hat{\rho}_\sigma \hat{\mathbf{u}}_\sigma)^T \right] \\
 &- \frac{\hat{e}_\sigma}{\hat{D}_\sigma} \hat{\rho}_\sigma (\hat{\mathbf{u}}_\sigma - \hat{\mathbf{u}})
 \end{aligned}$$

$$\alpha_{\sigma\nu}^{II} = \frac{\lambda_{m\nu}^{II}}{\lambda_{\sigma\nu}^{II} + \lambda_{m\nu}^{II}}, \quad \hat{D}_\sigma = \frac{1}{3 \hat{\lambda}_m^I}, \quad \hat{\nu}_{\sigma m} = \frac{1}{3 (\hat{\lambda}_{\sigma\nu}^{II} + \hat{\lambda}_{m\nu}^{II})}$$





Consistency at Macroscopic Level: MIP

- MIP: summing the governing equations for the single species should yield the mixture equations governing the **total density** and the **barycentric velocity**



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$$\sum_{\sigma} \left[(1 - \alpha_{\sigma\nu}^{II}) \hat{\rho}_{\sigma} \hat{\mathbf{u}}_{\sigma} \otimes \hat{\mathbf{u}}_{\sigma} + \alpha_{\sigma\nu}^{II} \hat{\rho}_{\sigma} \hat{\mathbf{u}} \otimes \hat{\mathbf{u}} \right] = \hat{\rho} \hat{\mathbf{u}} \otimes \hat{\mathbf{u}}$$

$$\text{diag}(\mathbf{D}_{\sigma}) = [0, 0, 0, \quad 0, 0, 0, \quad \lambda_{\sigma}^{III}, \lambda_{\sigma}^{III}, \lambda_{\sigma}^{IV}]^T$$

$$\text{diag}(\mathbf{D}_m) = [0, \lambda_m^I, \lambda_m^I, \quad \lambda_{m\nu}^{II}, \lambda_{m\nu}^{II}, \lambda_{m\eta}^{II}, \quad \lambda_m^{III}, \lambda_m^{III}, \lambda_m^{IV}]^T$$

- It is clear from the previous example that **MIP** \subset **μ IP** \rightarrow In fact the macroscopic formulation of the Indifferentiability Principle refers only to the **hydrodynamic moments**



MRT Gross & Krook Model

- Dropping out the first collisional operator, we find AGAIN the **corrected Gross & Krook model (CGK)**, BUT powered by the **MRT flexibility** → **This model satisfies the Indifferentiability Principle !!!**

$$\frac{D\mathbf{f}_\sigma}{Dt} = \mathbf{A}_m [\mathbf{f}_m^e(\rho_\sigma, \mathbf{u}, m_\sigma) - \mathbf{f}_\sigma]$$

$$m_\sigma = m \rightarrow \sum_\sigma \mathbf{f}_m^e(\rho_\sigma, \mathbf{u}, m_\sigma) = \mathbf{f}_m^e(\rho, \mathbf{u}, m)$$

$$\frac{D\mathbf{f}}{Dt} = \mathbf{A}_m [\mathbf{f}_m^e(\rho, \mathbf{u}, m) - \mathbf{f}]$$

- It is possible to tune independently the **kinematic viscosity ν** and the **diffusion coefficient D** (i.e. to tune the **Schmidt number $Sc = \nu / D$**) (Asinari, PRE 2006)





Different Particle Masses: Velocity Space



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$$f_m^e(\mathbf{u}) = \frac{\rho_\sigma}{m_\sigma (2\pi e_\sigma)^{D/2}} \exp \left[-\frac{(\mathbf{v} - \mathbf{u})^2}{2 e_\sigma} \right]$$

$$e_\sigma = RT/M_\sigma, e_\sigma = c_\sigma^2/3 \rightarrow c_\sigma = \delta x_\sigma / \delta t$$

- Particles with different molecular weights move at different lattice speeds when at the same temperature → **Different streaming distances** are employed for species with different molecular weights (Abraham & McCracken, PRE 2005)
- **Computational expensive** because of the additional interpolations due to managing multiple meshes



Different Particle Masses: Moment Space

- Design of the equilibrium distribution function in the velocity space for tuning the speed of sound is not very successful (Abraham & McCracken, PRE 2005)
- **Direct design of the equilibrium distribution function in the moment space** is better (particle mass effects the pressure only and not the other moments)

$$2\text{D lattice } \{ \hat{u}_x^n \hat{u}_y^m \} \rightarrow \mathbf{M}$$

$$\mathbf{m}_m^e = \mathbf{M} \mathbf{f}_m^e(\mathbf{u}, s_\sigma) = \hat{\rho}_\sigma [1, \hat{u}_x, \hat{u}_y, \hat{u}_x \hat{u}_y, s_\sigma/3 + \hat{u}_x^2, s_\sigma/3 + \hat{u}_y^2, 0, 0, 0]^T$$

$$e_\sigma = s_\sigma c^2 / 3$$

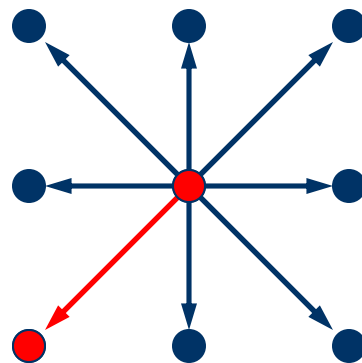
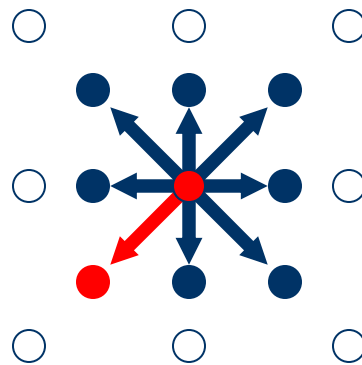
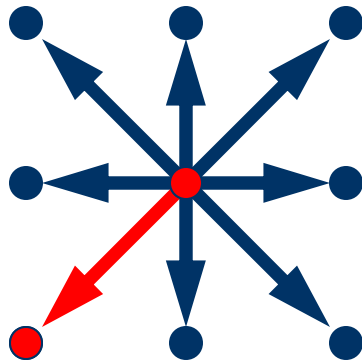




Physical Interpretation of Direct Design 1



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Multi-Lattice Approach:
the heavier particles are characterized by a slower dynamics and they need a finer mesh

Single-Lattice Approach:
all the species move on the same lattice but the moving heavier particles are fewer



Physical Interpretation of Direct Design 2

- The correction factor is simply proportional to the ratio between the number of **moving particles** and the **total number of particles** in equilibrium conditions

$$\gamma = \frac{\sum_{\hat{\mathbf{v}}_k \neq 0} \mathbf{f}_m^e |k}{\sum_k \mathbf{f}_m^e |k} = \frac{5}{9} s_\sigma \rightarrow s_\sigma \leq 1$$

- For stability reasons, it is better not to increase this ratio more than the usual definition \rightarrow The unique **lattice must match the dynamics of the fastest species** \rightarrow All the species diffuse according to molecular weight

$$-\frac{s_\sigma}{3 \hat{\lambda}_m^I} \hat{\nabla} \hat{\rho}_\sigma = \hat{\rho}_\sigma (\hat{\mathbf{u}}_\sigma - \hat{\mathbf{u}})$$



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Dealing with High Schmidt Number

- An important feature of LBM is that it allows us to model **high Reynolds number flows** by means of relaxation frequencies which imply **moderate round-off errors**

$$\hat{\nu}_m = \frac{1}{3 \hat{\lambda}_{m\nu}^{II}} - \frac{1}{6}$$

$$O(\hat{\lambda}_{m\nu}^{II}) = 1, \quad \lim_{\hat{\lambda}_{m\nu}^{II} \rightarrow 2^-} \hat{\nu}_m = 0^+$$

- Similarly dealing with the concentration driven diffusion term, **the discrete effect can be constructively used**

$$-s_\sigma \left(\frac{1}{3 \hat{\lambda}_m^I} - \frac{1}{6} \right) \hat{\nabla} \hat{\rho}_\sigma = \hat{\rho}_\sigma (\hat{\mathbf{u}}_\sigma - \hat{\mathbf{u}})$$





Consistency in Mixture Diffusion

- Any (multi-fluid) numerical scheme for mixture modeling must ensure the **same diffusion coefficient** in BOTH the **concentration equation** and the **diffusive flux definition** → otherwise the continuity is not satisfied ☹

$$\frac{\partial \hat{\rho}_\sigma}{\partial \hat{t}} + \hat{\nabla} \cdot (\hat{\rho}_\sigma \hat{\mathbf{u}}) = D_\sigma^T \hat{\nabla}^2 \hat{\rho}_\sigma$$

$$\hat{D}_\sigma^F \hat{\nabla} \hat{\rho}_\sigma = -\hat{\rho}_\sigma (\hat{\mathbf{u}}_\sigma - \hat{\mathbf{u}})$$

$$\frac{\partial \hat{\rho}_\sigma}{\partial \hat{t}} + \hat{\nabla} \cdot \left[\hat{\rho}_\sigma \hat{\mathbf{u}} + \frac{D_\sigma^T}{\hat{D}_\sigma^F} \hat{\rho}_\sigma (\hat{\mathbf{u}}_\sigma - \hat{\mathbf{u}}) \right] = 0$$

- It is not possible to hide additional terms due to discrete errors of the numerical scheme in the **concentration equation**, without changing accordingly the **diffusive flux definition** as well





Species Velocity Correction

- A proper correction of the single species velocity is required for ensuring that the **correct continuity equation** and the **desired flux definition** are recovered

$$\hat{\mathbf{u}}_{\sigma}^{*} = \hat{\mathbf{u}}_{\sigma} + n \hat{\mathbf{w}}_{\sigma} \rightarrow n = -\hat{\lambda}_m^I / 2$$

$$\frac{\partial \hat{\rho}_{\sigma}}{\partial \hat{t}} + \hat{\nabla} \cdot \left[\hat{\rho}_{\sigma} \hat{\mathbf{u}}_{\sigma}^{*} + \hat{\rho}_{\sigma} \hat{\mathbf{w}}_{\sigma}^{*} \left(\frac{\hat{\lambda}_m^I / 2 + n}{1 + n} \right) \right] = 0$$

$$s_{\sigma} / 3 \hat{\nabla} \hat{\rho}_{\sigma} = -\hat{\rho}_{\sigma} \left(\frac{\hat{\lambda}_m^I}{1 + n} \right) \hat{\mathbf{w}}_{\sigma}^{*}$$





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Diffusion Process at Macroscopic Level



Macroscopic Diffusion Model

- The proposed model is consistent with the macroscopic diffusion model of **Stefan–Maxwell** in the continuous regime
- This model correctly takes into account the effects due to both **concentration** and **total pressure gradients** (the acceleration effects are neglected here)
- It can be considered an extension of the **Fick model**

$$\lambda_m^I (\tilde{\mathbf{u}}_A - \tilde{\mathbf{u}}_B) = - \frac{\tilde{p} \tilde{\rho}}{\tilde{\rho}_A \tilde{\rho}_B} \mathbf{d}_{AB}$$

$$\mathbf{d}_{AB} = \nabla y_A + \frac{\tilde{n}_A \tilde{n}_B (M_B - M_A)}{\tilde{\rho} \tilde{n}} \nabla \tilde{n}$$



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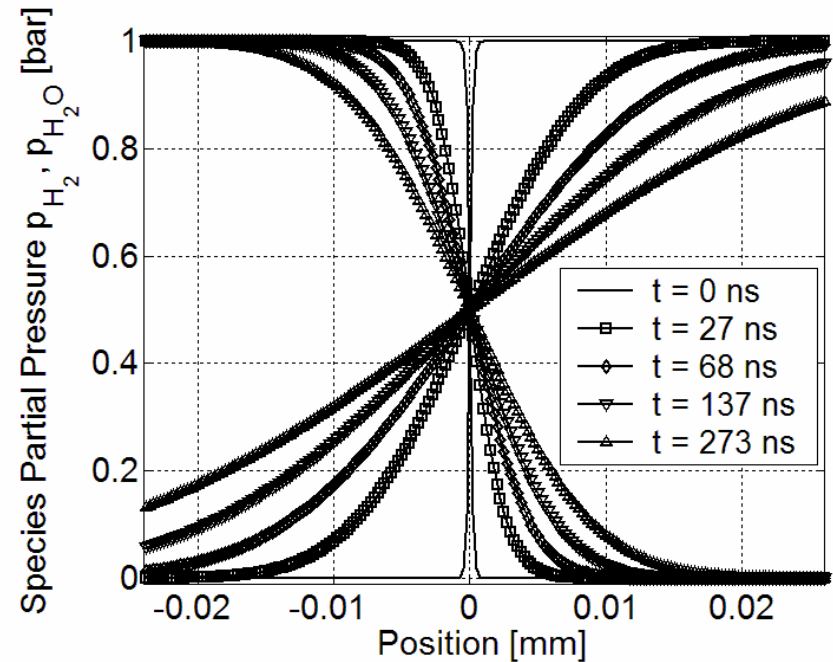
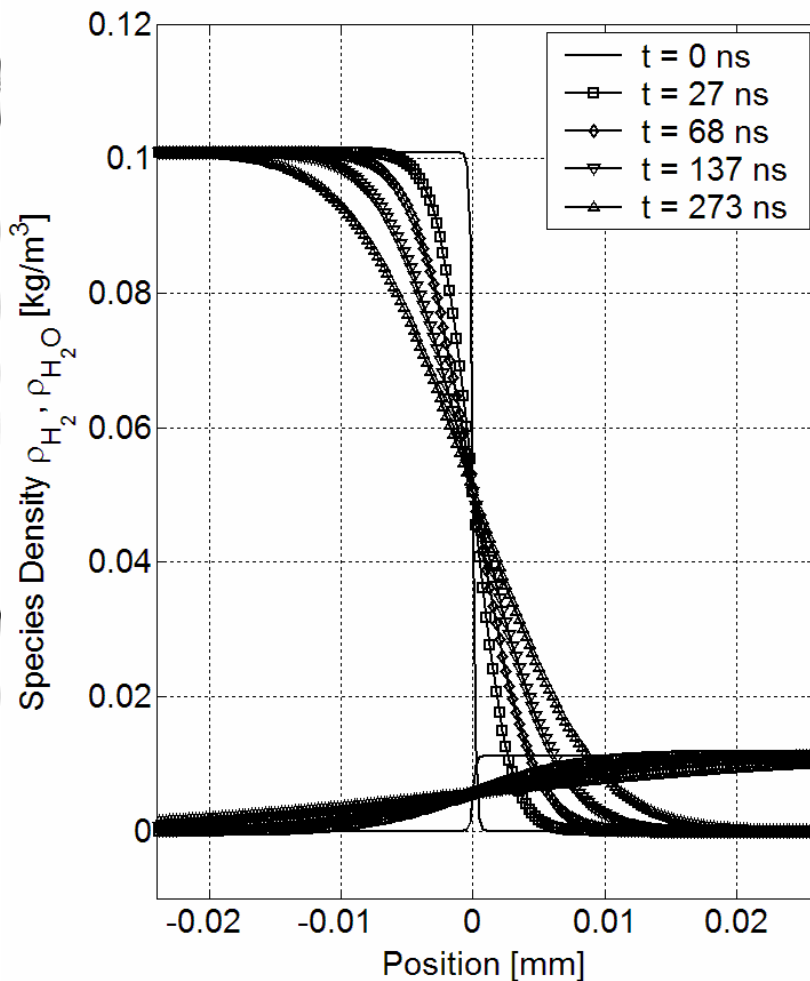


Simple Test Case: Fick Model

- Binary mixture made of water and hydrogen ($M_A/M_B=9/1$).
- Barycentric velocity dynamics is neglected \rightarrow no baroclinic back coupling.



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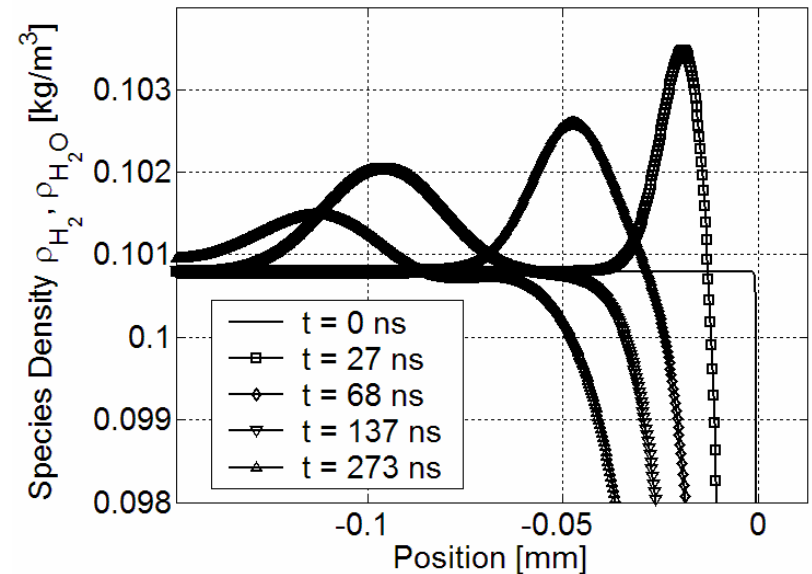
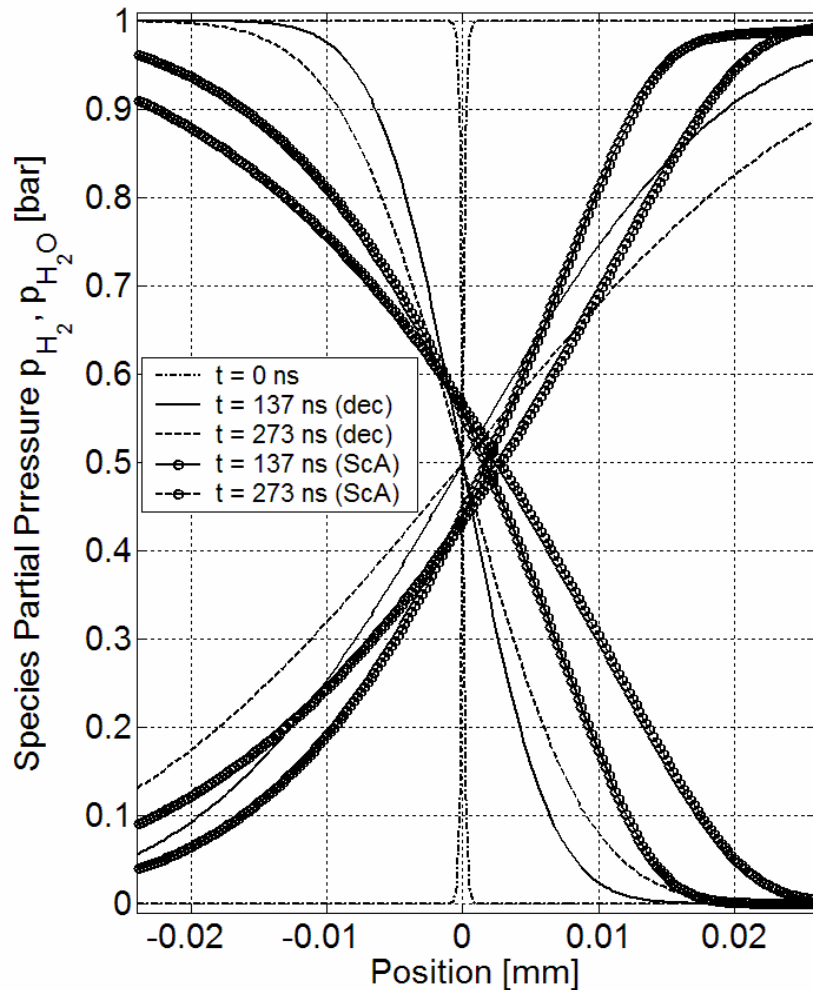


Simple Test Case: Maxwell-Stefan Model

- **Baroclinic back coupling** induces an additional drag effect.
- Small **concentration overshoots** driven by fast perturbations appear.



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Approaches to Mixing Modeling

- Mixing phenomena can be classified in different categories, according to the interaction between transported quantities and main flow dynamics (Dimotakis, Annu. Rev. Fluid Mech. 2005):
 - **Passive Scalar (PS)**, meaning that such mixing does not couple back on the flow dynamics (density-matched gasses, trace markers, ...);
 - **Active Scalar (AS)**, meaning that such mixing is actively effecting the flow dynamics (baroclinic effect, concentration-driven viscous coupling...);
 - **Reactive Active Scalar (RAS)**, which means that such mixing produces changes in the nature of the fluids (combustion, thermonuclear, ...).





Baroclinic Effect

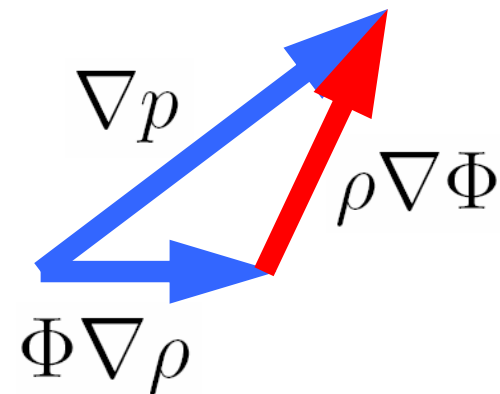
- **Baroclinic effect** derives from misalignments between pressure and density gradients or, equivalently, mass concentration and/or temperature gradients in the flow.



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$$p = RT \left(\frac{\rho_A}{M_A} + \frac{\rho_B}{M_B} \right) = \Phi \rho$$

$$\Phi = RT \left(\frac{x_A}{M_A} + \frac{x_B}{M_B} \right)$$



- The barycentric Φ is **no more a constant** (like it happens for the single species) \rightarrow The gradient of Φ depends on the single species dynamics (**baroclinic back coupling – BBC**).



Concentration – Dependent Viscosity

- The cross collisions effect the effective kinematic viscosity for the mixture, which is **smaller than the averaged viscosity based on the mass concentrations of the components**

$$\nu = \frac{x_a \nu_a}{1 + F_{ab} y_b / y_a} + \frac{x_b \nu_b}{1 + F_{ba} y_a / y_b} \leq \sum_{\sigma} x_{\sigma} \nu_{\sigma}$$

- The kinematic viscosity for the mixture is **no more a constant** (like it happens for the single species) → The gradient of the mixture kinematic viscosity depends on the single species dynamics (**viscous back coupling – VBC**)



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Semi-implicit Discretization Strategies



(Usual) Explicit Forward Euler

- A very popular formulation of LBM is based on the **forward Euler rule (FE)** because it is very simple and explicit in time

$$\begin{aligned} \vec{\mathbf{f}}_{\sigma}(\hat{t}_c + 1, \hat{\mathbf{X}}_c + \hat{\mathbf{V}}) - \mathbf{f}_{\sigma}(\hat{t}_c, \hat{\mathbf{x}}_c) &= \hat{\mathbf{A}}_m [\mathbf{f}_m^{e0}(\hat{t}_c, \hat{\mathbf{x}}_c) \\ &+ \mathbf{f}_m^{e1}(\hat{t}_c, \hat{\mathbf{x}}_c) + \mathbf{f}_m^{e2}(\hat{t}_c, \hat{\mathbf{x}}_c) - \mathbf{f}_{\sigma}(\hat{t}_c, \hat{\mathbf{x}}_c)] \end{aligned}$$

- Asymptotic analysis suggests that the most complicated **(non-linear) terms** may be solved by a **smaller accuracy (!!)**

$$O(\mathbf{f}_m^{e0}) = O(\hat{\mathbf{u}}_{\sigma}^0) = \epsilon^0$$

$$O(\mathbf{f}_m^{e1}) = O(\hat{\mathbf{u}}_{\sigma}^1) = \epsilon^1$$

$$O(\mathbf{f}_m^{e2}) = O(\hat{\mathbf{u}}_{\sigma}^2) = \epsilon^2$$



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Semi-implicit Linearized Backward Euler

- Semi-implicit linearized backward Euler (**SILBE**) formulation: the basic idea is **to solve implicitly all the linear terms** and **explicitly only the quadratic term**

$$\mathbf{f}_\sigma(\hat{t}_c, \hat{\mathbf{x}}_c) - \vec{\mathbf{f}}_\sigma(\hat{t}_c - 1, \hat{\mathbf{X}}_c - \hat{\mathbf{V}}) = \hat{\mathbf{A}}_m [\mathbf{f}_m^{e0}(\hat{t}_c, \hat{\mathbf{x}}_c) + \mathbf{f}_m^{e1}(\hat{t}_c, \hat{\mathbf{x}}_c) + \mathbf{f}_m^{e2}(\hat{t}_c - 1, \hat{\mathbf{x}}_c) - \mathbf{f}_\sigma(\hat{t}_c, \hat{\mathbf{x}}_c)]$$

- The data of the previous time step are used for computing the quadratic part only: the algorithm is completely local (**only the neighboring cells** are involved as usual) because the linear operators can be **inverted once for ALL the cells** → there is no need to solve a large linear system of equations



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Crank – Nicolson Approach

- Asymptotic analysis allows us to verify that the leading discrete errors due to the previous schemes (FE and BE) **differ only for the sign** → It seems natural to combine them for achieving better performances → **parallel** (with regards to time) **Crank – Nicolson**



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$$\begin{aligned} \left[\vec{\mathbf{f}}_{\sigma} \right]_{(\hat{t}_c+1)}^{FE} &= \mathbf{f}_{\sigma}(\hat{t}_c, \hat{\mathbf{x}}_c) + \hat{\mathbf{A}}_m \left[\mathbf{f}_m^e(\hat{t}_c, \hat{\mathbf{x}}_c) - \mathbf{f}_{\sigma}(\hat{t}_c, \hat{\mathbf{x}}_c) \right] \\ \left[\vec{\mathbf{f}}_{\sigma} - \hat{\mathbf{A}}_m (\mathbf{f}_m^{e0} + \mathbf{f}_m^{e1} - \mathbf{f}_{\sigma}) \right]_{(\hat{t}_c+1)}^{BE} &= \mathbf{f}_{\sigma}(\hat{t}_c, \hat{\mathbf{x}}_c) + \hat{\mathbf{A}}_m \mathbf{f}_m^{e2}(\hat{t}_c, \hat{\mathbf{x}}_c) \\ \left[\vec{\mathbf{f}}_{\sigma} \right]_{(\hat{t}_c+1)}^{CN} &= 1/2 \left[\vec{\mathbf{f}}_{\sigma} \right]_{(\hat{t}_c+1)}^{FE} + 1/2 \left[\vec{\mathbf{f}}_{\sigma} \right]_{(\hat{t}_c+1)}^{BE} \end{aligned}$$

- Because of the time–space coupling of LBM, **in-series hybrid schemes** force to consider **refined meshes**

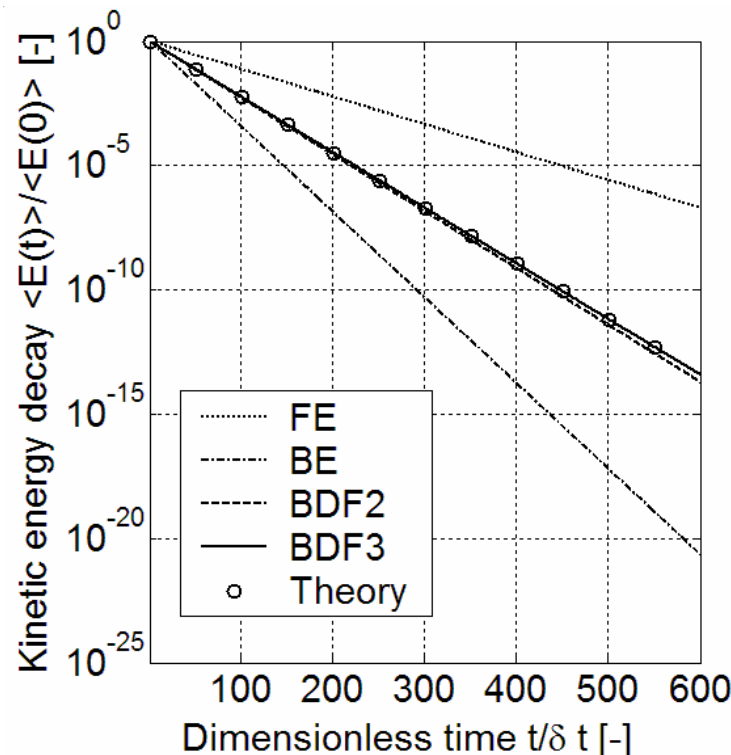


Is Crank – Nicolson Approach Useful ?

- Not for conventional single-species hydrodynamics: the (FE-)LBM is already second order accurate (in space) because the discrete error is included in the definition of the effective transport coefficient



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Taylor-Green vortex

$$\hat{\nu}_{\sigma m}^{FE} = \frac{1}{3 \hat{\lambda}_{m\nu}^{II}} - \frac{1}{6}$$

$$\hat{\nu}_{\sigma m}^{CN} = \frac{1}{3 \hat{\lambda}_{m\nu}^{II}}$$

$$\hat{\nu}_{\sigma m}^{BE} = \frac{1}{3 \hat{\lambda}_{m\nu}^{II}} + \frac{1}{6}$$



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Application: Direct Numerical Simulation (DNS) of Decaying Homogenous Isotropic Turbulence (DHIT)



DNS of DHIT for a Binary Mixture

- Direct numerical simulation (DNS) of **decaying homogenous isotropic turbulence** (DHIT) for a binary mixture
- **Divergence-free** momentum fields are **randomly generated** for each species according to a given **energy spectrum**:

$$i\mathbf{k} \cdot \hat{\mathbf{j}}_{\sigma}(\mathbf{k}) = 0 \quad \hat{E}(\mathbf{k}, 0) = E(k) \in [k_{min}, k_{MAX}]$$

- **Kinetic energy** and **dissipation function** are computed during the decay for analysing the late time dynamics

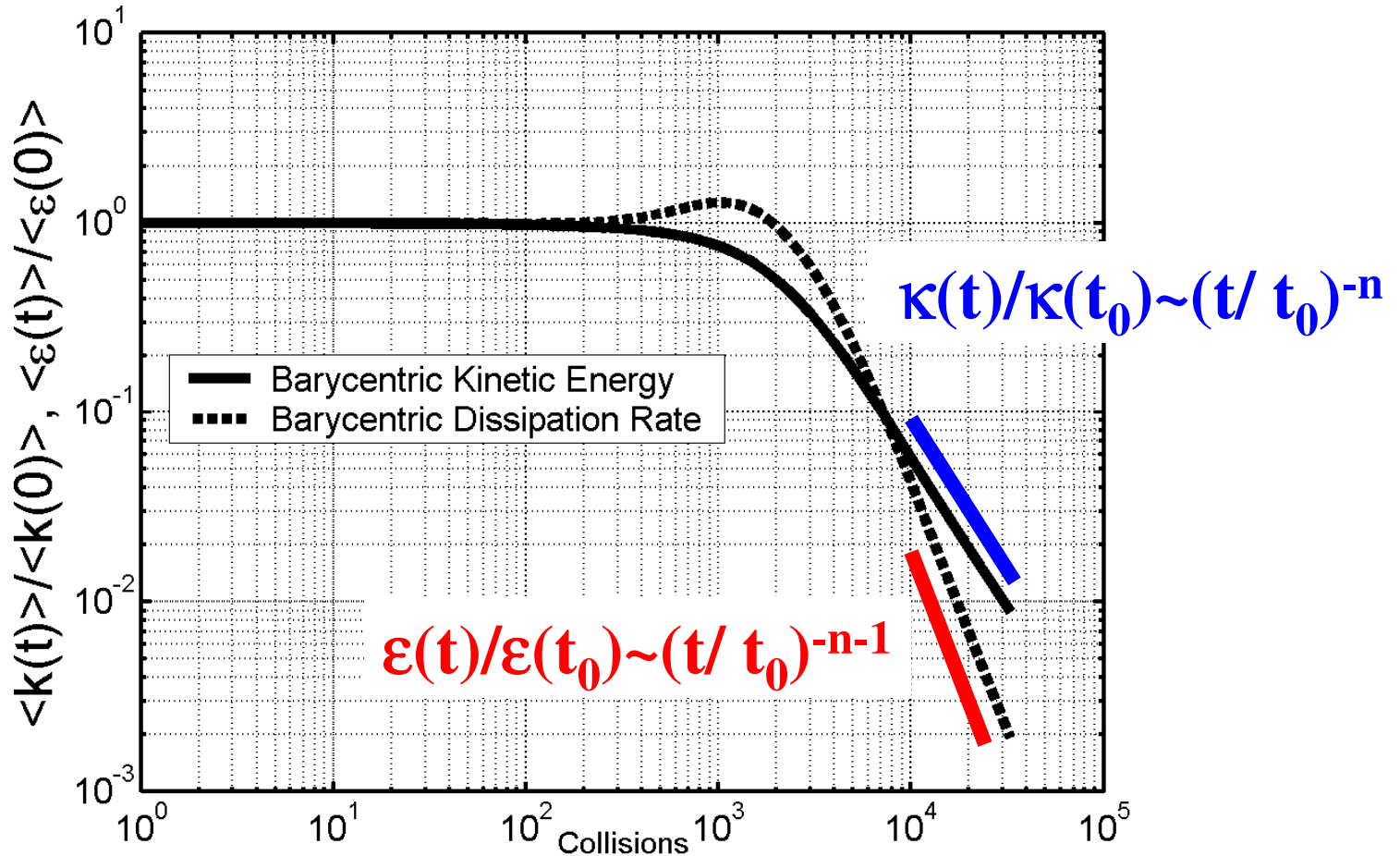
$$\kappa(t) = \int \hat{E}(\mathbf{k}, t) d\mathbf{k} \quad \epsilon(t) = 2\nu \int \mathbf{k}^2 \hat{E}(\mathbf{k}, t) d\mathbf{k}$$





Asymptotic Power-Law Decay

Binary mixture, mesh size 135^3 , $E(k) = 0.038 k^4 \exp(-0.14 k^2)$ with $k \in [4,8]$

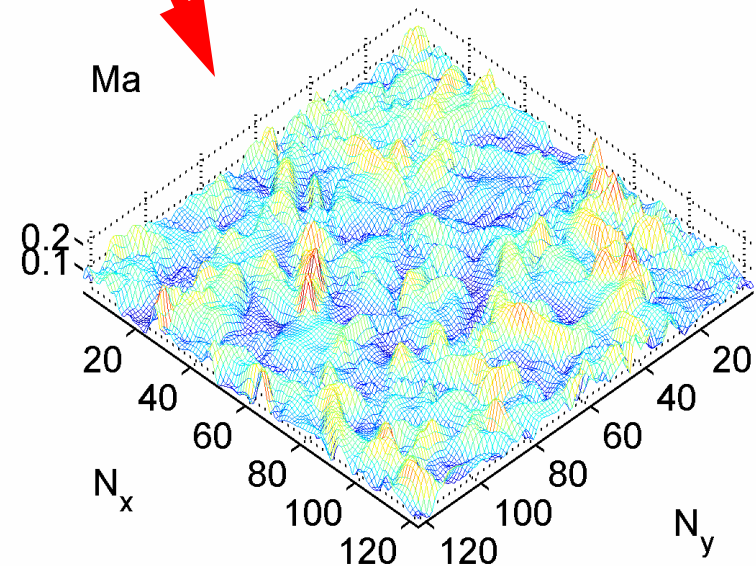
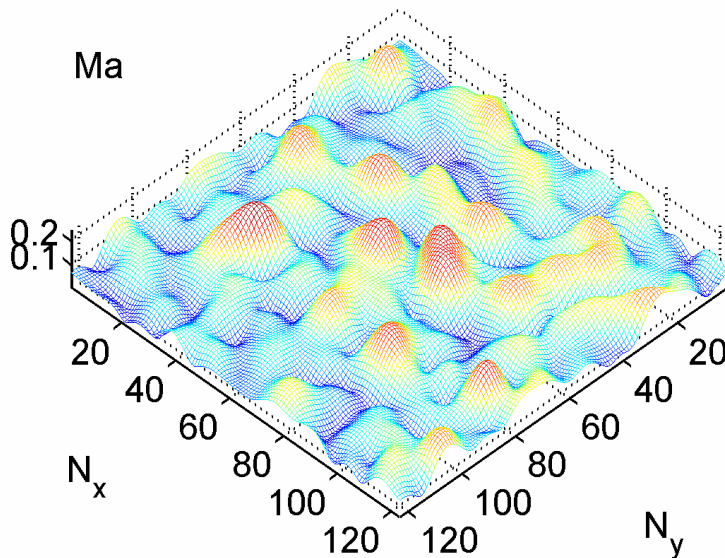
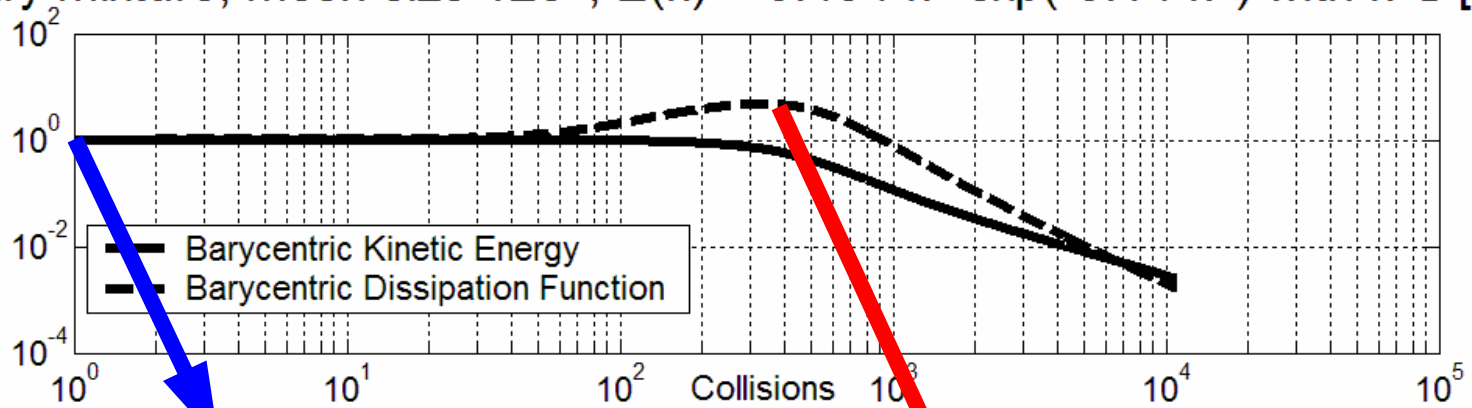


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Dissipative Eddies

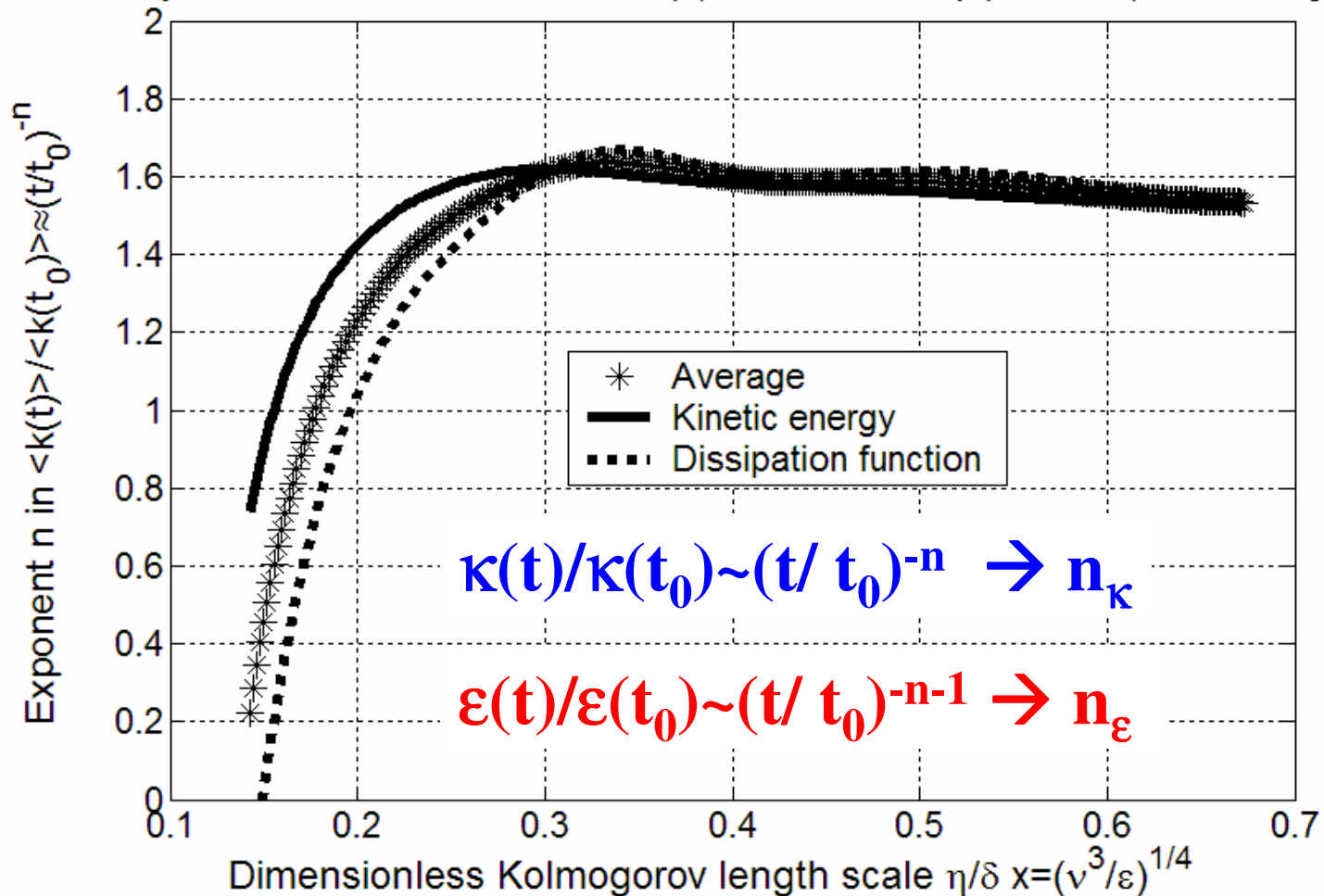
Binary mixture, mesh size 123^3 , $E(k) = 0.494 k^4 \exp(-0.14 k^2)$ with $k \in [1,8]$





Kolmogorov Length Scale

Binary mixture, mesh size 135^3 , $E(k) = 0.038 k^4 \exp(-0.14 k^2)$ with $k \in [4, 8]$



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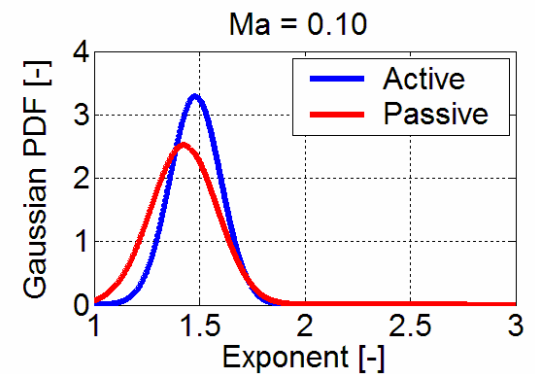
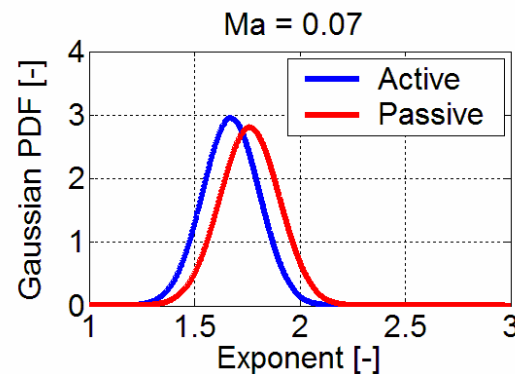
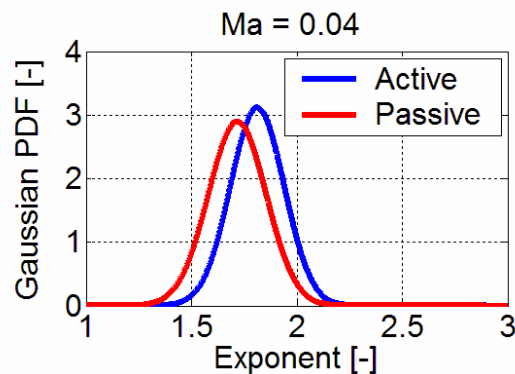


Baroclinic Effect on Decay Dynamics

- (1): $E(k,0) = 0.038 k^4 \exp(-0.14 k^2)$, $k \in [1,4]$ on 63^3
- (2): $E(k,0) = 0.608 k^4 \exp(-0.56 k^2)$, $k \in [2,4]$ on 63^3
- (3): $E(k,0) = 0.494 k^4 \exp(-0.14 k^2)$, $k \in [1,8]$ on 123^3
- As far as the **low Mach number limit** is concerned (values up to 0.1 have been considered), the baroclinic effect **does not substantially change the decay**.



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Summary and Outlook

- The **consistency** of the physical model (at microscopic level and consequently at macroscopic level) should be one of the key concept leading the design process of LB schemes for mixture modeling
- **MRT Corrected Gross & Krook (CGK) model** is acceptably **consistent**, **flexible** (tunable Schmidt number) and **robust** (if you need more robustness → semi-implicit or implicit schemes may be considered)
- **Baroclinic** and **viscous back couplings** (i.e. the single species dynamics effecting the barycentric dynamics) may appear in **shock interactions of mixtures** because of the **large concentration gradients** → This phenomena could be further investigated by shock capturing schemes (like Gas Kinetic Schemes)





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