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# Randomization of Uncertain Systems: A New Paradigm for Robust Control

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- Additional documents, papers, etc, please consult

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- Some MATLAB<sup>TM</sup> codes are available at

<http://www.polito.it/~dabbene>



- Preliminaries
- Randomized Algorithms for Analysis
- Probabilistic Robust Synthesis
- Randomized Algorithms for Optimal Control (LQR)
- Probabilistic LPV Systems
- Applications
  1. High Speed Networks
  2. Control of Mini UAV



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# Preliminaries

# Randomized Algorithms (RAs)

- Randomized algorithms are frequently used in many areas of engineering, computer science, physics, finance, optimization,...but their appearance in systems and control is mostly limited to Monte Carlo simulations...
- **Main objective of this tutorial:** Introduction to rigorous study of RAs for uncertain systems and control, with specific applications

# Randomized Algorithms (RAs)

- Combinatorial optimization, computational geometry
- **Examples:** Data structuring, search trees, graph algorithms, sorting, ...
- Motion and path planning problems
- Mathematics of finance: Computation of path integrals
- Bioinformatics (string matching problems)



- “Randomized Algorithms” by R. Motwani and P. Raghavan, Cambridge University Press, 1995
- “Randomized Algorithms for Analysis and Control of Uncertain Systems” by R. Tempo, G. Calafiore and F. Dabbene, Springer, 2005

- Uncertainty has been always a critical issue in control theory and applications
- First methods to deal with uncertainty were based on a **stochastic** approach
- Optimal control: LQG and Kalman filter
- Since early 80's alternative **deterministic** approach (worst-case or robust) has been proposed



- Major stepping stone in 1981: Formulation of the  $\mathcal{H}_\infty$  problem by George Zames
- Various “robust” methods to handle uncertainty now exist: Structured singular values, Kharitonov, optimization-based (LMI),  $l_1$ -optimal control, quantitative feedback theory (QFT)



- Late 80's and early 90's: Robust control theory became a well-assessed area
- Successful industrial applications in aerospace, chemical, electrical, mechanical engineering, ...
- However, ...

# Limitations of Robust Control - 1

- Researchers realized some drawbacks of robust control
- Consider uncertainty  $\Delta$  bounded in a set  $\mathcal{B}$  of radius  $\rho$ . Largest value of  $\rho$  such that the systems is stable for all  $\Delta \in \mathcal{B}$  is called (worst-case) **robustness margin**
- **Conservatism**: Worst case robustness margin may be small
- **Discontinuity**: Worst case robustness margin may be discontinuous wrt problem data

## Limitations of Robust Control - 2

- **Computational Complexity:** Worst case robustness is often  $\mathcal{NP}$ -hard (not solvable in polynomial time unless  $\mathcal{P} = \mathcal{NP}$ )<sup>[1]</sup>
- Various robustness problems are  $\mathcal{NP}$ -hard
  - static output feedback
  - structured singular value
  - stability of interval matrices

[1] V. Blondel and J.N. Tsitsiklis (2000)

# Conservatism and Complexity Trade-Off

- Uncertain or control design parameters often enter into the system in a nonlinear/nonconvex fashion
- To avoid complexity issues (or just to find a solution of the problem) **relaxation** techniques such as SOS are used
- Study issues about the accuracy of the approximation introduced and related complexity

# Different Paradigm Proposed

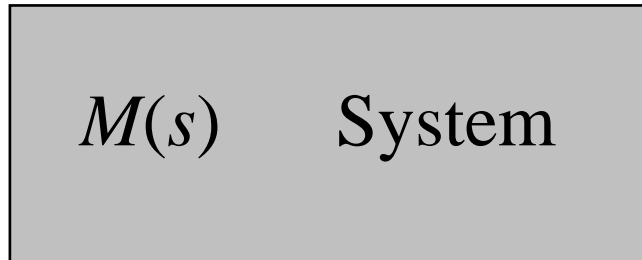
- New paradigm proposed is based on uncertainty randomization and leads to **randomized algorithms** for analysis and synthesis
- Within this setting a different notion of problem tractability is needed
- **Objective:** Breaking the curse of dimensionality<sup>[1]</sup>

[1] R. Bellman (1957)

# Probability *and* Robustness

- The interplay of **Probability** and **Robustness** for control of uncertain systems
- **Robustness**: Deterministic uncertainty bounded
- **Probability**: Random uncertainty (pdf is known)
- Computation of the probability of performance
- Controller which stabilizes *most* uncertain systems

- We obtain larger robustness margins at the expense of a small risk
- We study the probability degradation *beyond* the robustness margins
- Computational complexity is generally not an issue: Randomized algorithms are low complexity



- $\Delta$  belongs to a structured set  $\mathcal{B}_D$ 
  - Parametric uncertainty  $q$
  - Nonparametric uncertainty  $\Delta_i$
  - Mixed uncertainty

- Worst case model: Set membership uncertainty
- The uncertainty  $\Delta$  is bounded in a set  $\mathcal{B}_D$

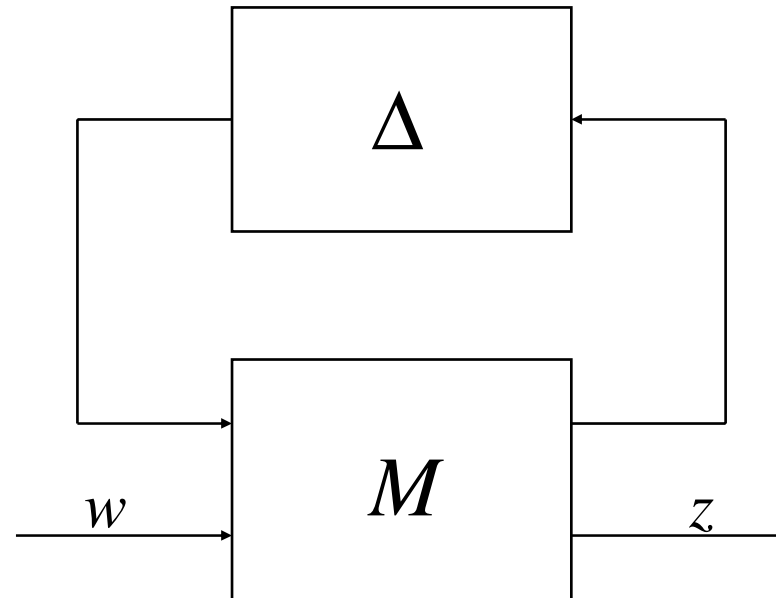
$$\Delta \in \mathcal{B}_D$$

- Real parametric uncertainty  $q=[q_1, \dots, q_\ell] \in \mathbb{R}^\ell$

$$q_i \in [q_i^-, q_i^+]$$

- Nonparametric uncertainty

$$\Delta_i \in \{\Delta_i \in \mathbb{R}^{n,n} : \|\Delta_i\| \leq 1\}$$



- Uncertainty  $\Delta$  is bounded in a structured set  $\mathcal{B}_D$
- $z = \mathcal{F}_u(M, \Delta) w$ , where  $\mathcal{F}_u(M, \Delta)$  is the upper LFT

# Objective of Robustness

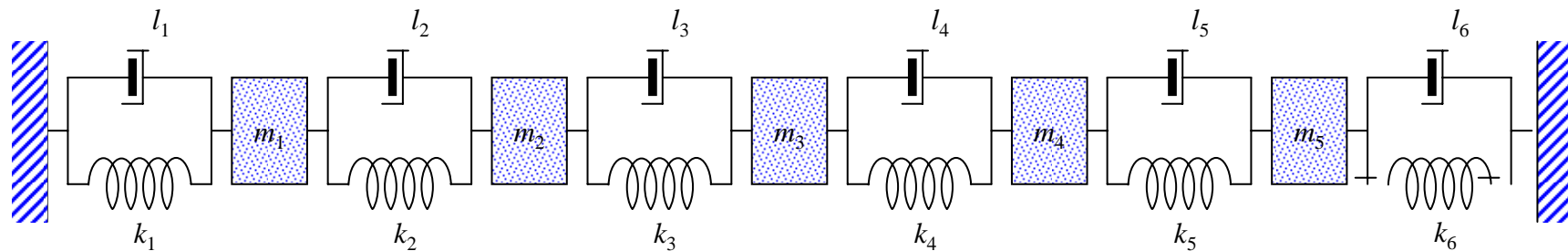
- Objective of **robustness**: To guarantee stability and performance for all

$$\Delta \in \mathcal{B}_D$$

- Different probabilistic paradigm based on uncertainty randomization of  $\Delta$  within  $\mathcal{B}_D$

# Example: Flexible Structure - 1

- Mass spring damper model
- Real parametric uncertainty affecting stiffness and damping
- Complex unmodeled dynamics (nonparametric)



- $M$ - $\Delta$  configuration for controlled systems and study stability of

$$M(s) = C(sI - A)^{-1}B$$

$$\Delta = \begin{bmatrix} q_1 I_5 & 0 & 0 \\ 0 & q_2 I_5 & 0 \\ 0 & 0 & \Delta_1 \end{bmatrix}$$

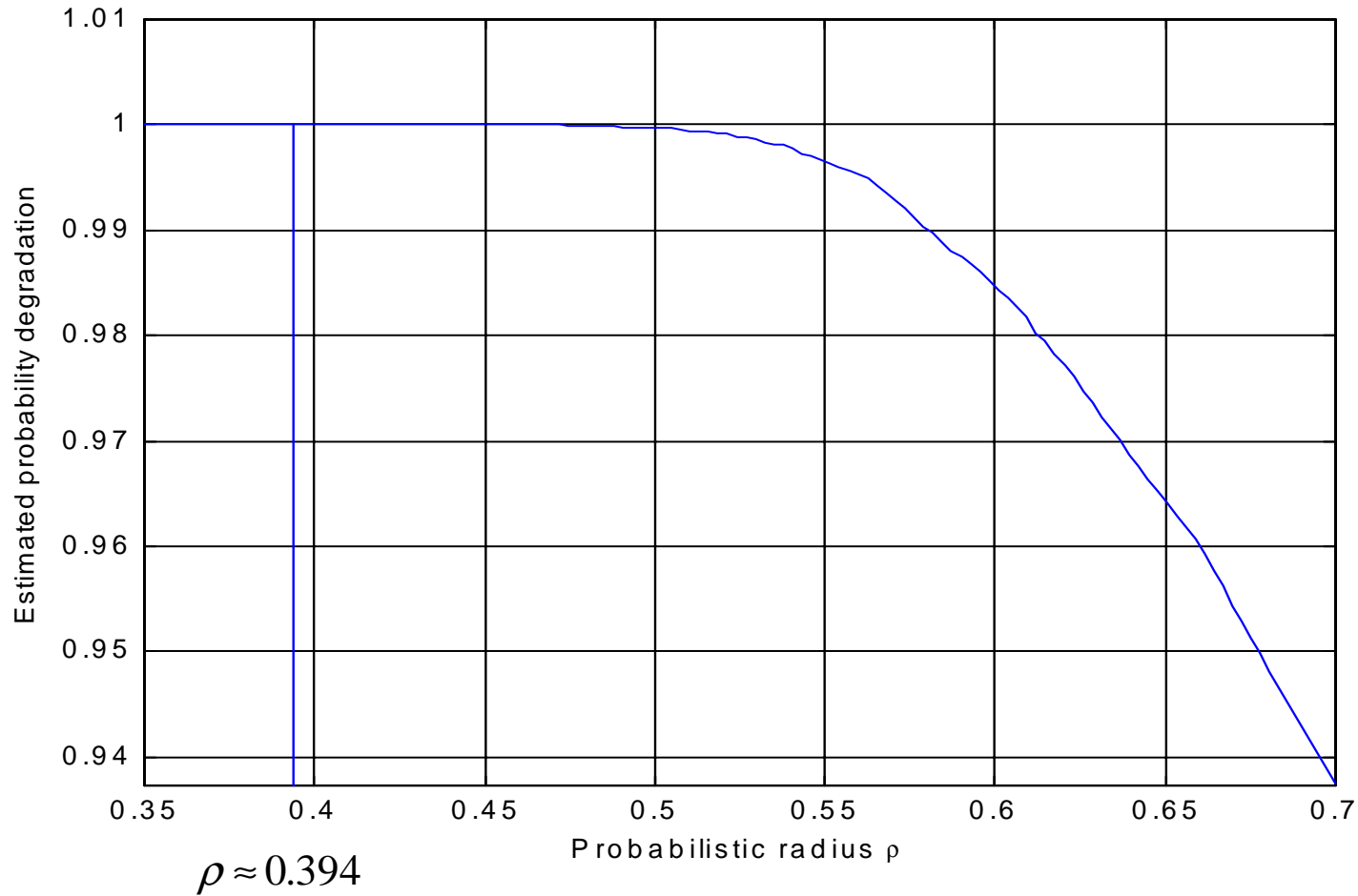
$$q_1, q_2 \in \mathbb{R}$$

$$\Delta_1 \in \mathbb{C}^{4,4}$$

$$\Delta \in \mathcal{B}_D = \{ \Delta \in \mathcal{D} : \sigma(\Delta) < \rho \}$$



# Probability Degradation Function





- Probability density function associated to  $\mathcal{B}_D$
- We now assume that  $\Delta$  is a random matrix with given density function  $f_{\Delta}(\Delta)$  and support  $\mathcal{B}_D$
- **Example:**  $\Delta$  is uniform in  $\mathcal{B}_D$



- Take  $f_{\Delta}(\Delta) = \mathcal{U}[\mathcal{B}_D]$  (uniform density within  $\mathcal{B}_D$ )

$$\mathcal{U}[\mathcal{B}_D] = \begin{cases} \frac{1}{\text{vol}(\mathcal{B}_D)} & \text{if } \Delta \in \mathcal{B}_D \\ 0 & \text{otherwise} \end{cases}$$

- In this case, for a subset  $\mathcal{S} \subseteq \mathcal{B}_D$

$$\Pr\{\Delta \in \mathcal{S}\} = \frac{\int_{\mathcal{S}} d\Delta}{\text{vol}(\mathcal{B}_D)} = \frac{\text{vol}(\mathcal{S})}{\text{vol}(\mathcal{B}_D)}$$

# Performance Function

- In classical robustness we guarantee that a certain performance requirement is attained for all  $\Delta \in \mathcal{B}_D$
- This can be stated in terms of a **performance function**

$$J = J(\Delta)$$

- **Examples:**  $\mathcal{H}_\infty$  performance and robust stability

## Example: $\mathcal{H}_\infty$ Performance - 1

- Compute the  $\mathcal{H}_\infty$  norm of the upper LFT  $\mathcal{F}_u(M, \Delta)$

$$J(\Delta) = \| \mathcal{F}_u(M, \Delta) \|_\infty$$

- For given  $\gamma > 0$ , check if

$$J(\Delta) < \gamma$$

for all  $\Delta$  in  $\mathcal{B}_D$

## Example: $\mathcal{H}_\infty$ Performance - 2

- Continuous time SISO systems with real parametric uncertainty  $q$  with upper LFT

$$\mathcal{F}_u(M, \Delta) = \mathcal{F}_u(M, q) =$$

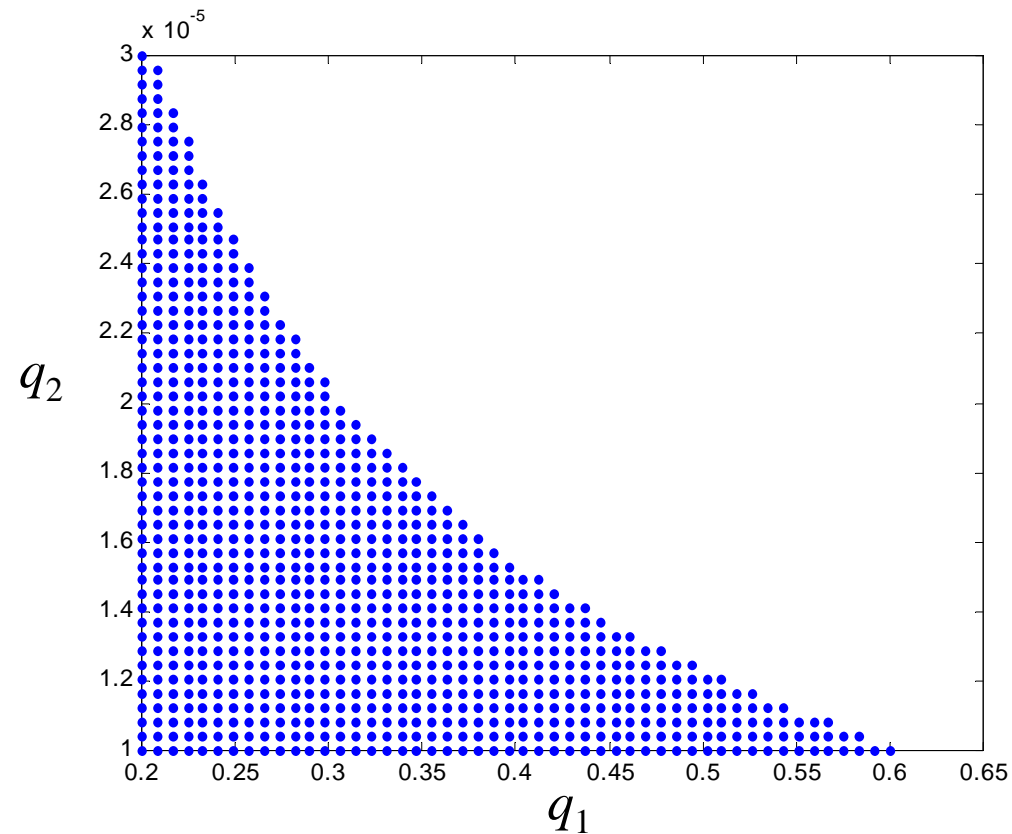
$$\frac{0.5q_1q_2s + 10^{-5}q_1}{(10^{-5} + 0.05q_2)s^2 + (0.00102 + 0.5q_2)s + (2 \cdot 10^{-5} + 0.5q_1^2)}$$

where  $q_1 \in [0.2, 0.6]$  and  $q_2 \in [10^{-5}, 3 \cdot 10^{-5}]$

- Letting  $J(q) = \|\mathcal{F}_u(M, q)\|_\infty$ , we choose  $\gamma=0.003$
- Check if  $J(q) < \gamma$  for all  $q$  in these intervals

## Example: $\mathcal{H}_\infty$ Performance - 3

- The set of  $q_1, q_2$  for which  $J(q) < \gamma$  is shown below



## Example<sup>[1]</sup>: Robust Stability - 1

- Consider the closed loop uncertain polynomial

$$p(s,q) =$$

$$(1 + r^2 + 6q_1 + 6q_2 + 2q_1q_2) + (q_1 + q_2 + 3)s + (q_1 + q_2 + 1)s^2 + s^3$$

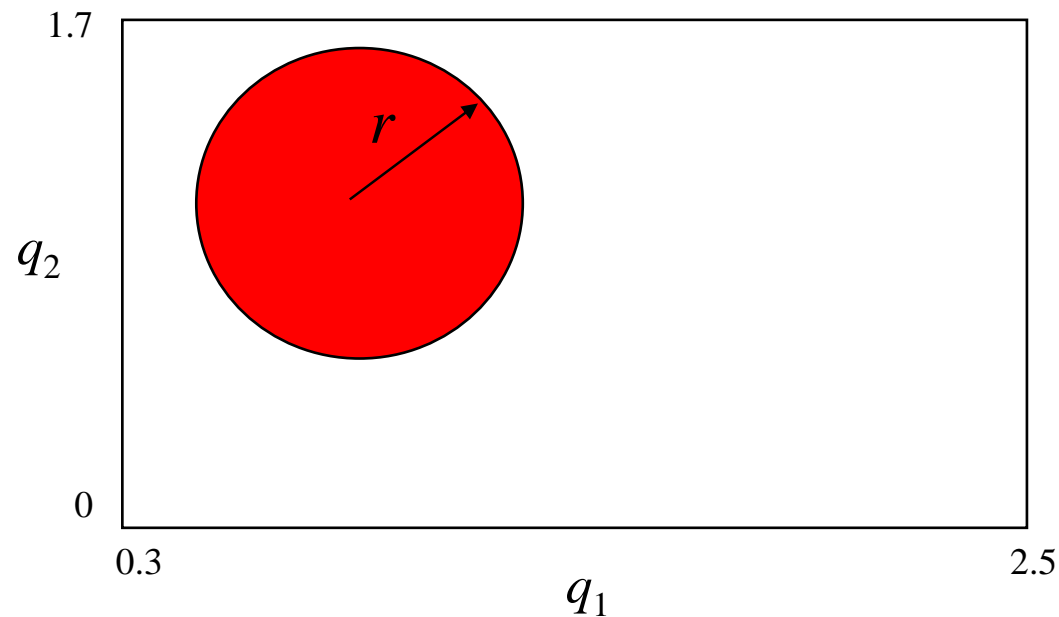
where  $q_1 \in [0.3, 2.5]$ ,  $q_2 \in [0, 1.7]$  and  $r=0.5$

- Check stability for all  $q$  in these intervals

[1] G. Truxal (1961)

## Example: Robust Stability - 2

- Set of unstable polynomials



- Taking  $r=0$  the unstable set reduces to a singleton

# P1: Performance Verification

- For given performance level  $\gamma$ , check whether

$$J(\Delta) \leq \gamma$$

for all  $\Delta$  in  $\mathcal{B}_D$



## P2: Worst-Case Performance



- Find  $J_{\max}$  such that

$$J_{\max} = \max_{\Delta \in \mathcal{B}_D} J(\Delta)$$



- We define two subsets of  $\mathcal{B}_D$

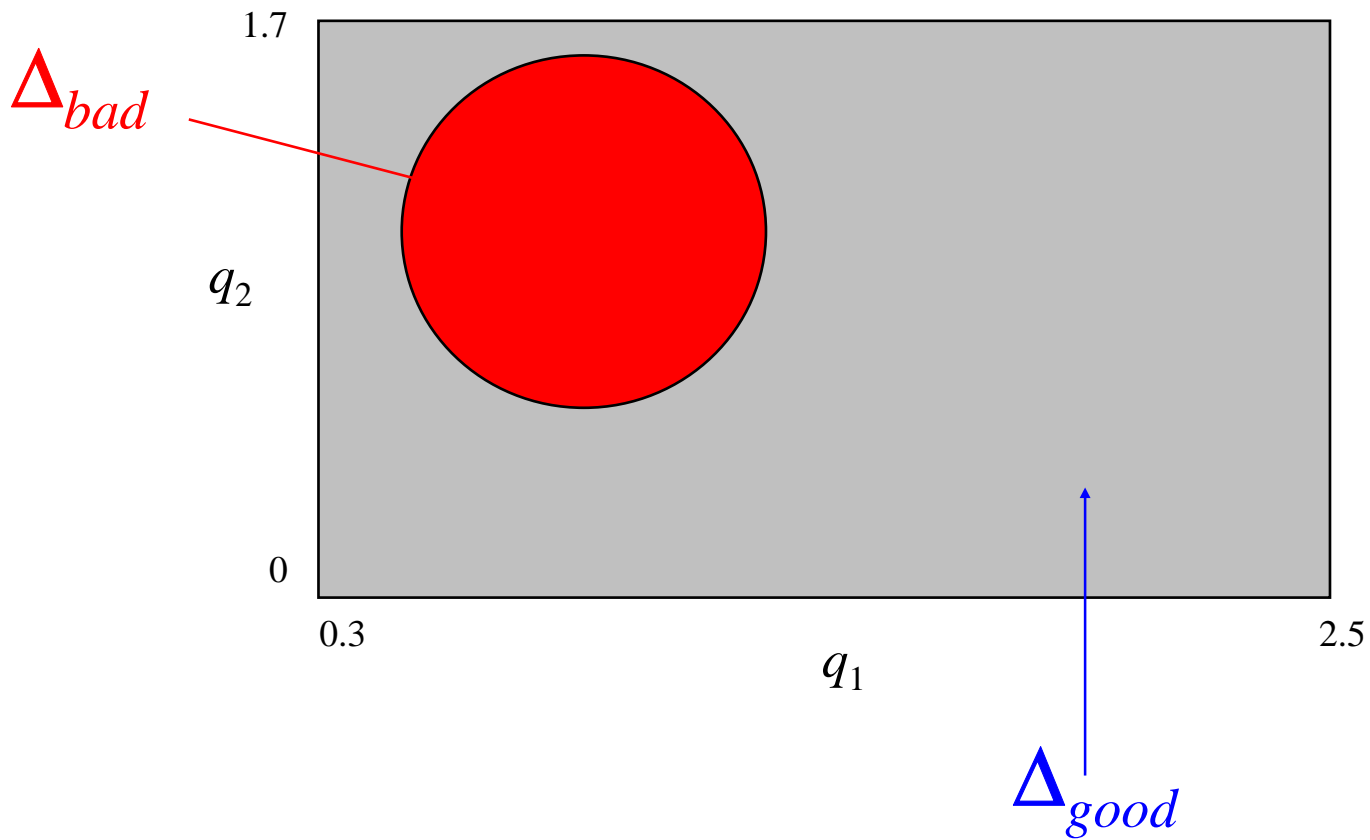
$$\Delta_{good} = \{ \Delta: J(\Delta) \leq \gamma \} \subseteq \mathcal{B}_D$$

$$\Delta_{bad} = \{ \Delta: J(\Delta) > \gamma \} \subseteq \mathcal{B}_D$$

- $\Delta_{good}$  is the set of  $\Delta$ 's satisfying performance
- Measure of robustness is

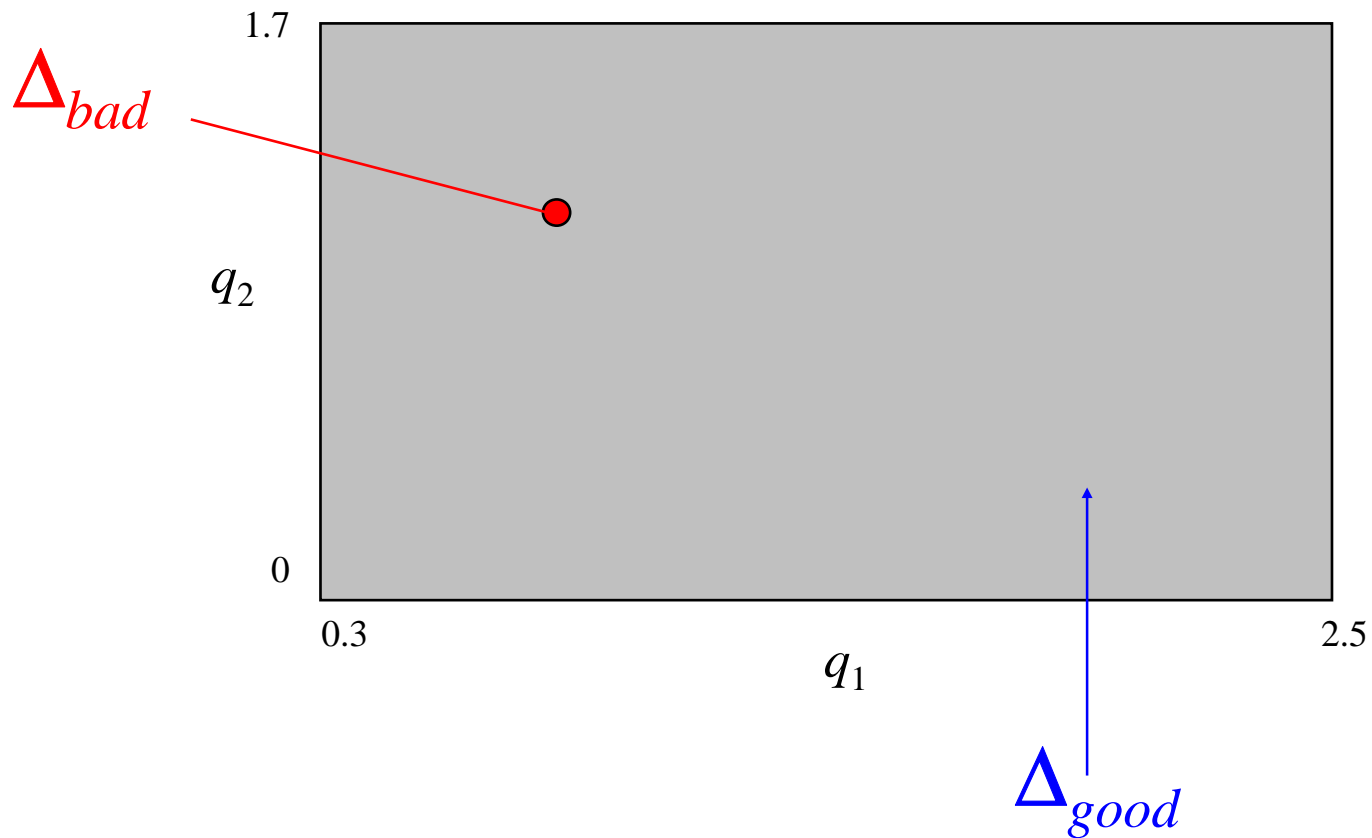
$$vol(\Delta_{good}) = \int_{\Delta_{good}} d\Delta$$

# Example of Good and Bad Sets



# Example of Good and Bad Sets - 2

Taking small  $r$



# Probabilistic Robustness Measure

- In worst-case analysis we compute  $\gamma$  such that **all**  $\Delta$  satisfy performance. Equivalently, we evaluate  $\gamma$  such that

$$\Delta_{good} = \mathcal{B}_D$$

- In a probabilistic setting, we are satisfied if the ratio

$$\frac{vol(\Delta_{good})}{vol(\mathcal{B}_D)}$$

is **close** to one

- We define the **probability of performance** as

$$p_\gamma = \Pr\{J(\Delta) \leq \gamma\}$$

- Notice that, if  $f_\Delta(\Delta)$  is uniform, then

$$p_\gamma = \frac{\text{vol}(\Delta_{\text{good}})}{\text{vol}(\mathcal{B}_D)}$$

[1] R.F. Stengel (1980)

## Example: Closed-Form Computation

- For Truxal's example, we compute  $p_\gamma$  in closed-form
- For uniform distribution, we have

$$\text{vol}(\Delta_{good}) = 3.74 - \pi r^2$$

$$\text{vol}(\mathcal{B}_D) = 3.74$$



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# Randomized Algorithms for Analysis

# Optimization versus Integration

- Robustness margin computation requires **optimization**
- Computation of  $p_\gamma$  requires **integration**
- We are switching from optimization to integration
- Computing multidimensional integrals is a difficult task
- Complexity of multidimensional integration<sup>[1]</sup>

[1] J.F. Traub, G.W. Wasilkowski and H. Wozniakowski (1988)

- Assume that  $\Delta$  is random with pdf  $f_{\Delta}(\Delta)$  with support  $\mathcal{B}_D$
- **Accuracy**  $\varepsilon \in (0,1)$  and **confidence**  $\delta \in (0,1)$  be assigned
- **Performance function** for analysis and **level**



$$J = J(\Delta)$$



$$\gamma$$

# Randomized Algorithms for Analysis

- Two classes of randomized algorithms for probabilistic robust performance analysis
- P1: Performance verification (compute  $p_\gamma$ )
- P2: Worst-case performance (compute  $J_{\max}$ )
- Both are based on uncertainty randomization of  $\Delta$
- Bounds on the sample size are obtained

- We estimate  $p_\gamma$  by means of a randomized algorithm
- First, we generate  $N$  i.i.d. samples

$$\Delta^1, \Delta^2, \dots, \Delta^N \in \mathcal{B}_D$$

according to the density  $f_\Delta$

- We evaluate  $J(\Delta^1), J(\Delta^2), \dots, J(\Delta^N)$

- Construct an indicator function

$$I(\Delta^i) = \begin{cases} 1 & \text{if } J(\Delta^i) \leq \gamma \\ 0 & \text{otherwise} \end{cases}$$

- An estimate of  $p_\gamma$  is the **empirical probability**

$$\hat{p}_N = \frac{1}{N} \sum_{i=1}^N I(\Delta^i) = \frac{N_{good}}{N}$$

where  $N_{good}$  is the number of samples such that  $J(\Delta^i) \leq \gamma$

- The empirical probability is a reliable estimate if

$$|p_\gamma - \hat{p}_N| = |\Pr\{J(\Delta) \leq \gamma\} - \hat{p}_N| \leq \varepsilon$$

- Find the minimum  $N$  such that

$$\Pr\{|p_\gamma - \hat{p}_N| \leq \varepsilon\} \geq 1 - \delta$$

where  $\varepsilon \in (0,1)$  and  $\delta \in (0,1)$



- For any  $\varepsilon \in (0,1)$  and  $\delta \in (0,1)$ , if

$$N \geq \frac{\log \frac{2}{\delta}}{2\varepsilon^2}$$

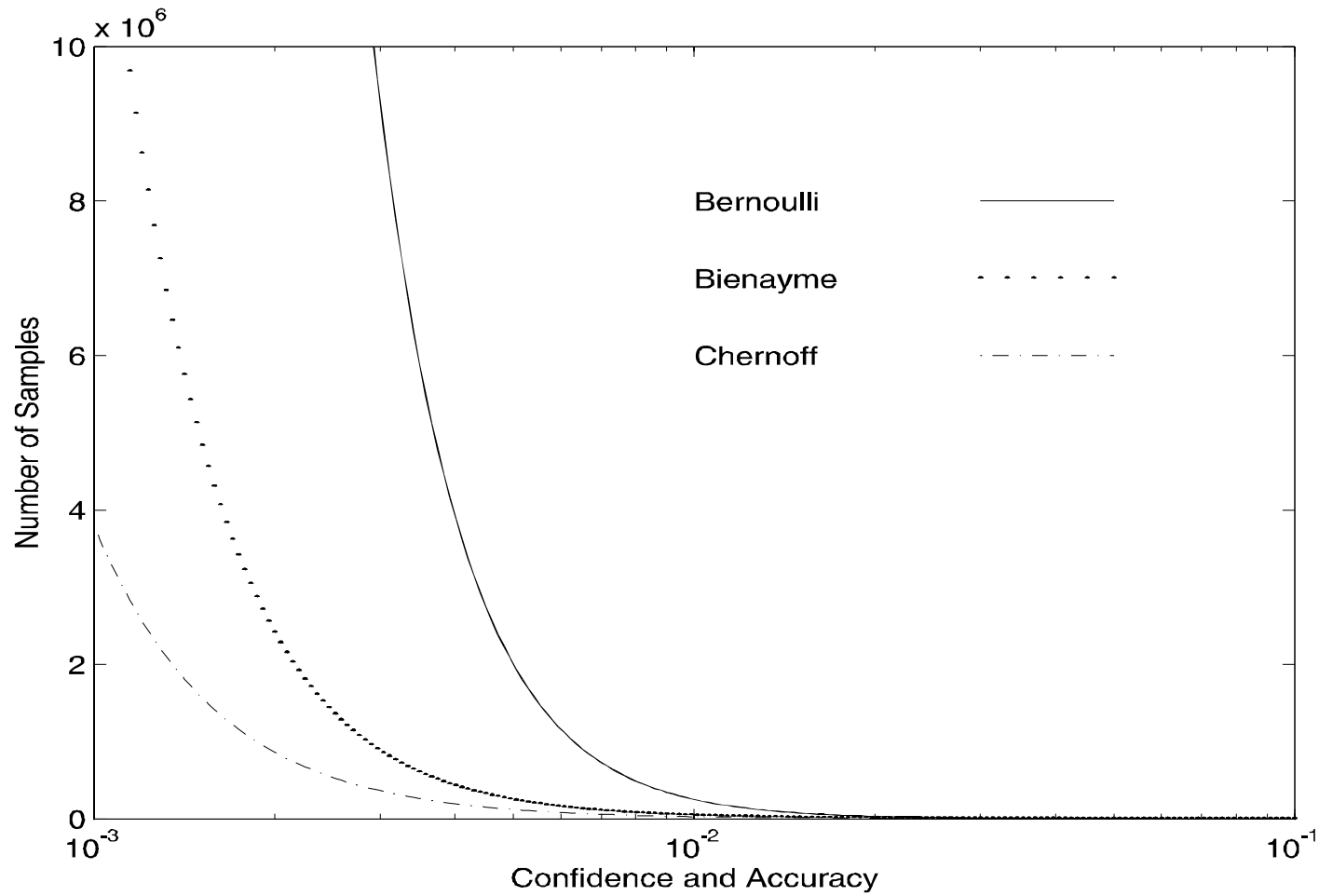
then

$$\Pr\{|p_\gamma - \hat{p}_N| \leq \varepsilon\} \geq 1 - \delta$$

[1] H. Chernoff (1952)



# Comparison Between Bounds





- **Remark:** Chernoff bound improves upon other bounds such as Bernoulli (Law of Large Numbers)
- Dependence on  $1/\delta$  is logarithmic
- Dependence on  $1/\varepsilon$  is quadratic

$\varepsilon$	0.1%	0.1%	0.5%	0.5%
$1-\delta$	99.9%	99.5%	99.9%	99.5%
$N$	$3.9 \cdot 10^6$	$3.0 \cdot 10^6$	$1.6 \cdot 10^6$	$1.2 \cdot 10^5$

# Computational Complexity of RAs

- RAs are **efficient** (polynomial-time) because
  1. Random sample generation of  $\Delta^i$  can be performed in polynomial-time
  2. Cost associated with the evaluation of  $J(\Delta^i)$  for fixed  $\Delta^i$  is polynomial-time
  3. Sample size is polynomial in the problem size and probabilistic levels  $\varepsilon$  and  $\delta$

# 1. Random Sample Generation

- Random number generation (RNG): Linear and nonlinear methods for uniform generation in  $[0,1)$  such as Fibonacci, feedback shift register, BBS, MT, ...
- Non-uniform univariate random variables: Suitable functional transformations (e.g., the inversion method)
- The problem is **much harder**: Multivariate generation of samples of  $\Delta$  with pdf  $f_{\Delta}(\Delta)$  and support  $\mathcal{B}_D$
- It can be resolved in polynomial-time



## 2. Cost of Checking Stability

- Consider a polynomial

$$p(s, a) = a_0 + a_1s + \cdots + a_ns^n$$

- To check left half plane stability we can use the Routh test. The number of multiplications needed is

$$\frac{n^2}{4} \text{ for } n \text{ even} \qquad \frac{n^2 - 1}{4} \text{ for } n \text{ odd}$$

- The number of divisions and additions is equal to this number
- We conclude that checking stability is  $O(n^2)$

## 3. Bounds on the Sample Size

- Chernoff bound is independent on the size of  $\mathcal{B}_D$ , on the structure  $\mathcal{D}$  on the number of blocks, on the pdf  $f_{\Delta}(\Delta)$
- It depends only on  $\delta$  and  $\varepsilon$
- Same comments can be made for other bounds such as Bernoulli



# Worst-Case Performance

- Recall that

$$J_{\max} = \max_{\Delta \in \mathcal{B}_D} J(\Delta)$$

- Generate  $N$  i.i.d. samples

$$\Delta^1, \Delta^2, \dots, \Delta^N \in \mathcal{B}_D$$

according to the density  $f_{\Delta}$

- Compute

$$\hat{J}_N = \max_{i=1..N} J(\Delta^i)$$

- For any  $\varepsilon \in (0,1)$  and  $\delta \in (0,1)$ , if

$$N \geq \frac{\log \frac{1}{\delta}}{\log \frac{1}{1-\varepsilon}}$$

then

$$\Pr\{\Pr\{J(\Delta) > \hat{J}_N\} \leq \varepsilon\} \geq 1 - \delta$$

[1] P.P. Khargonekar and A. Tikku (1996)

[2] R. Tempo, E. W. Bai and F. Dabbene (1996)

## Comparison and Comments

- Number of samples is much smaller than Chernoff
- Bound is a specific instance of the fpras (fully polynomial randomized approximated scheme) theory
- Dependence on  $1/\varepsilon$  is basically linear  $\left( \log \frac{1}{1-\varepsilon} \approx \varepsilon \right)$

$\varepsilon$	0.1%	0.1%	0.5%	0.5%	0.01%	0.001%
$1-\delta$	99.9%	99.5%	99.9%	99.5%	99.99%	99.999%
$N$	$6.91 \cdot 10^3$	$5.30 \cdot 10^3$	$1.38 \cdot 10^3$	$1.06 \cdot 10^3$	$9.21 \cdot 10^4$	$1.16 \cdot 10^6$

- In the case of  $f_{\Delta}(\Delta)$  uniform, we have

$$\Pr\{J(\Delta) > \hat{J}_N\} = \frac{\text{vol}(\Delta_{bad})}{\text{vol}(\mathcal{B}_D)}$$

- Therefore

$$\Pr\{\Pr\{J(\Delta) > \hat{J}_N\} \leq \varepsilon\} \geq 1 - \delta$$

is equivalent to

$$\Pr\{\text{vol}(\Delta_{bad}) \leq \varepsilon \text{vol}(\mathcal{B}_D)\} \geq 1 - \delta$$



# Confidence Intervals

- The Chernoff and worst-case bounds can be computed *a-priori* and are explicit
- The sample size obtained with the confidence intervals is not explicit
- Given  $\delta \in (0,1)$ , upper and lower confidence intervals  $p_L$  and  $p_U$  are such that

$$\Pr\{p_L \leq p_\gamma \leq p_U\} = 1 - \delta$$



## Confidence Intervals - 2

- The probabilities  $p_L$  and  $p_U$  can be computed *a posteriori* when the value of  $N_{good}$  is known, solving equations of the type

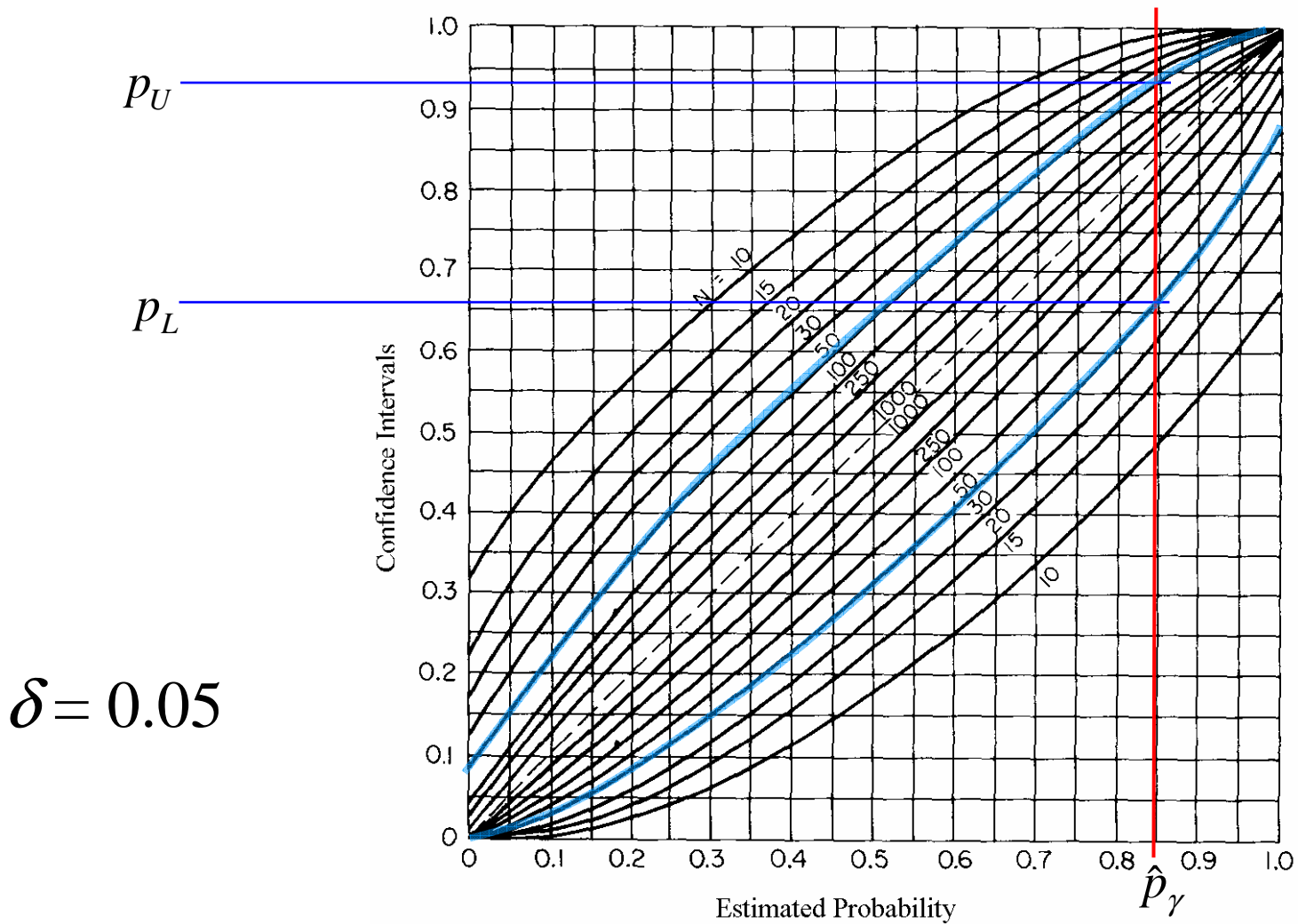
$$\sum_{k=N_{good}}^N \binom{N}{k} p_L^k (1-p_L)^{N-k} = \delta_L$$

$$\sum_{k=0}^{N_{good}} \binom{N}{k} p_U^k (1-p_U)^{N-k} = \delta_U$$

with  $\delta_L + \delta_U = \delta$



# Confidence Intervals - 3



- The Chernoff Bound studies the problem

$$\Pr\{|p_\gamma - \hat{p}_N| \leq \varepsilon\} \geq 1 - \delta$$

where  $p_\gamma = \Pr\{J(\Delta) \leq \gamma\}$

- Performance function  $J$  is fixed
- Computational Learning Theory computes bounds on the sample size for the problem

$$\Pr\{|\Pr(J(\Delta) \leq \gamma) - \hat{p}_N| \leq \varepsilon, \forall J \in \mathcal{J}\} \geq 1 - \delta$$

where  $\mathcal{J}$  is a given class of functions

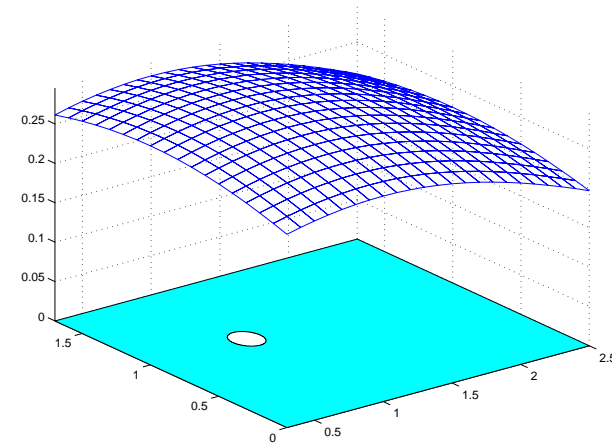
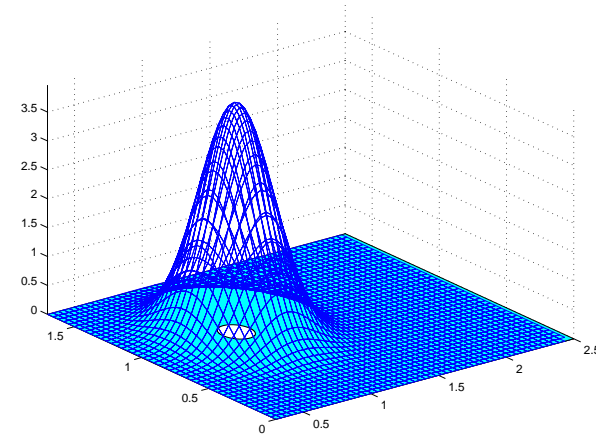
- Computation Learning Theory aims at studying **uniform** Law of Large Numbers
- The bounds obtained depend on quantities called VC-dimension (if  $J$  is a binary valued function), or P-dimension (if  $J$  is a continuous valued function)
- VC and P-dimension are measures of the problem complexity
- The bounds obtained are **very conservative**

[1] M. Vidyasagar (1997)

[2] E.D. Sontag (1998)

# Choice of the Distribution - 1

- The probability  $\Pr\{\Delta \in \mathcal{S}\}$  depends on  $f_{\Delta}(\Delta)$
- It may vary between 0 and 1 depending on the pdf  $f_{\Delta}(\Delta)$





## Choice of the Distribution - 2

- The bounds discussed are independent on the choice of the distribution but for computing  $\Pr\{J(\Delta) \leq \gamma\}$  we need to know the distribution  $f_{\Delta}(\Delta)$
- Some research has been done in order to find the worst-case distribution in a certain class<sup>[1]</sup>
- Uniform distribution is the worst-case if a certain target is convex and centrally symmetric

[1] B. R. Barmish and C. M. Lagoa (1997)



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## Choice of the Distribution - 3



- Minimax properties of the uniform distribution have been shown<sup>[1]</sup>

[1] E. W. Bai, R. Tempo and M. Fu (1998)



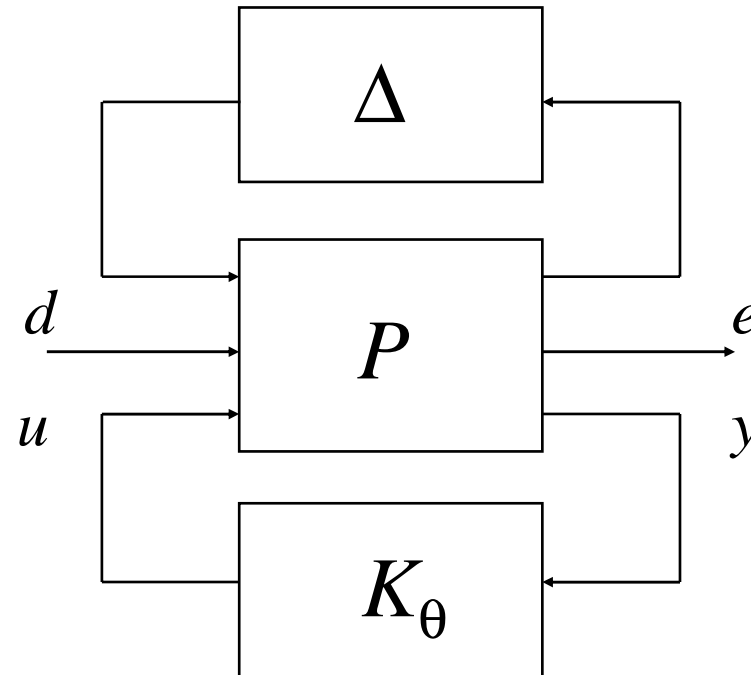
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# Probabilistic Robust Synthesis

# Analysis vs Design with Uncertainty

- Starting point: Worst-case analysis versus design
- Consider an interval family  $p(s,q)$ ,  $q \in \mathcal{B}_q = \{q \in \mathbb{R}^n, \|q\|_\infty \leq 1\}$
- **Analysis problem:**
  - Check if  $p(s,q)$  is stable for all  $q \in \mathcal{B}_q$   
Answer: Kharitonov Theorem
- **Design Problem:**
  - Does there exist a  $q \in \mathcal{B}_q$  such that  $p(s,q)$  is stable?  
Answer: *Unknown* in general



- Design the parameterized controller  $K_\theta$  to guarantee stability and performance

# Synthesis Performance Function

- Recall that the parameterized controller is  $K_\theta$
- We replace  $J(\Delta)$  with a **synthesis performance function**

$$J = J(\Delta, \theta)$$

where  $\theta \in \Theta$  represents the controller parameters to be determined and their bounding set

# Randomized Algorithms for Synthesis

- Two classes of RAs for probabilistic synthesis
- Average performance synthesis<sup>[1]</sup>
- Based on expected value minimization
- Utilization of computational learning theory results
- Very general problems can be handled
- Sample complexity bounds are very conservative and controller randomization is required

[1] M. Vidyasagar (1998)

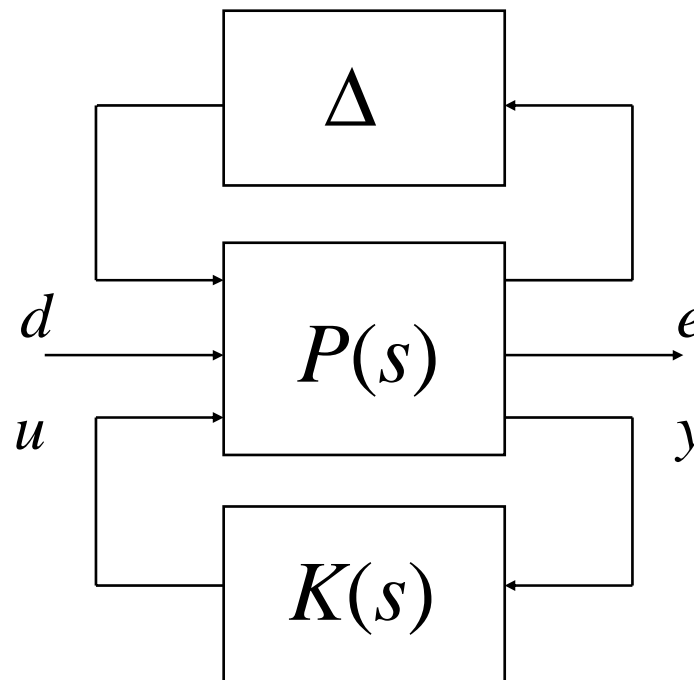
# Randomized Algorithms for Synthesis

- Robust performance synthesis<sup>[1]</sup>
- Problem reformulation as robust feasibility
- Only control convex problems can be handled
- Finite-time convergence with probability one is obtained

[1]B. Polyak and R. Tempo (2001)

# Robust Performance Synthesis

- Uncertainty randomization of  $\Delta$  in  $\mathcal{B}_D$
- Convex optimization to design the controller  $K(s)$





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# RAs for Optimal Control (LQR)

# Uncertain Systems in State Space

- We consider a state space description of the **uncertain system**

$$\dot{x}(t) = A(\Delta)x(t) + Bu(t)$$

with  $x(0)=x_0$ ;  $x \in \mathbb{R}^n$ ;  $u \in \mathbb{R}^m$ ,  $\Delta \in \mathcal{B}_D$

- For example,  $A(\Delta)$  is an interval matrix with bounded entries  $a_{ij}^- \leq a_{ij} \leq a_{ij}^+$

- The performance index is the **quadratic cost function**

$$J = \int_0^{\infty} (x^T S x + u^T R u) dt$$

where  $S > 0$  and  $R > 0$  are given weights

- The state feedback controller is

$$u = -R^{-1} B^T Q^{-1} x$$

where  $Q = Q^T > 0$  is solution of a QMI

# Quadratic Matrix Inequality

- Find  $Q=Q^T >0$  such that, for given  $0 \leq \gamma \leq 1$ ,

$$A(\Delta)Q + QA^T(\Delta) - 2BR^{-1}B^T + \gamma(QSQ + BR^{-1}B^T) \leq 0$$

for all  $\Delta \in \mathcal{B}_D$

- Then, the cost

$$J \leq \frac{1}{\gamma} x_0^T Q^{-1} x_0$$

is guaranteed for all  $\Delta \in \mathcal{B}_D$

# Robust Quadratic Stabilization

- Quadratic stabilization and **guaranteed cost** can be reduced to checking a finite number of matrix inequalities
- **Example:** If  $A(\Delta)$  is an interval matrix and  $R=I$ , for quadratic stabilization we take  $\gamma = 0$  and we need to find a solution  $Q=Q^T >0$  of

$$A^i Q + Q(A^i)^T - 2 BB^T \leq 0$$

for all vertex matrices  $A^i$

# Probabilistic Quadratic Stabilization

- **Critical problem:** The number of LMIs is too large and not tractable with classical interior point methods
- **Example:** If  $A(\Delta)$  is an interval matrix the number of LMIs is equal to the number of vertex matrices

$$N_V = 2^{n^2}$$

- Probabilistic version of quadratic stabilization and LQ regulator

- Randomly generate  $\Delta^1, \dots, \Delta^N \in \mathcal{B}_D$ . Then, check if the

LMI

$$A^i Q + Q(A^i)^T - 2 B B^T \leq 0$$

is feasible for  $i=1, \dots, N$  and find a **common solution**

$$Q = Q^T > 0$$

- **Critical problem:** Even if  $N$  is relatively small, this is a hard computational problem

- **Key point:** Sequential algorithm which deals with one constraint at each step
- At step  $k$  we have
  - Phase 1: Uncertainty randomization of  $\Delta$
  - Phase 2: Gradient algorithm and projection
- **Final result:** Find a solution  $Q=Q^T >0$  with probability one in a finite number of steps



- Let  $\mathcal{E}_n$  be an Euclidean space

$$\mathcal{E}_n = \left\{ A = A^T \in \mathbb{R}^n, \|A\| = \sqrt{\sum_{i,k=1}^n a_{1k}^2} \right\}$$

and  $C$  be the cone of positive semi-definite matrices

$$C = \{A \in \mathcal{E}_n : A \geq 0\}$$

- For any real symmetric matrix  $A$  we define the projection  $[A]^+ \in C$  as

$$[A]^+ = \arg \min_{X \in C} \|A - X\|$$

- The projection can be computed through the eigenvalue decomposition  $A = T\Lambda T^T$
- Then

$$[A]^+ = T\Lambda^+ T^T$$

where  $\lambda_i^+ = \max \{ \lambda_i, 0 \}$

## Phase 1: Uncertainty Randomization

- Uncertainty randomization: Generate  $\Delta^k \in \mathcal{B}_D$
- Then, for guaranteed cost we obtain the QMI

$$A(\Delta^k)Q + QA^T(\Delta^k) - 2BR^{-1}B^T + \gamma(QSQ + BR^{-1}B^T) \leq 0$$

- Define a matrix valued function

$$V(Q, \Delta^k) = A(\Delta^k)Q + QA^T(\Delta^k) - 2BR^{-1}B^T + \gamma(QSQ + BR^{-1}B^T)$$

and a scalar function

$$v(Q, \Delta^k) = \left\| [V(Q, \Delta^k)]^+ \right\|$$

where  $\| \cdot \|$  is the Frobenius norm

- We can also take the maximum eigenvalue of  $V(Q, \Delta^k)$

## Phase 2: Gradient Algorithm

- We write

$$Q^{k+1} = \begin{cases} [Q^k - \mu^k \partial_Q \{v(Q^k, \Delta^k)\}]^+ & \text{if } v(Q^k, \Delta^k) > 0 \\ Q^k & \text{otherwise} \end{cases}$$

where  $\partial_Q$  is the subgradient and the stepsize  $\mu^k$  is

$$\mu^k = \frac{v(Q^k, \Delta^k) + r \|\partial_Q \{v(Q^k, \Delta^k)\}\|}{\|\partial_Q \{v(Q^k, \Delta^k)\}\|^2}$$

and  $r > 0$  is a parameter

## Closed-form Gradient Computation

- The function  $v(Q, \Delta^k)$  is convex in  $Q$  and its subgradient is given by

$$\partial_Q \{v(Q, \Delta^k)\} =$$

$$\frac{[V(Q, \Delta^k)]^+ (A(\Delta^k) + \gamma QS) + (A(\Delta^k) + \gamma QS)^T [V(Q, \Delta^k)]^+}{v(Q, \Delta^k)}$$

if  $v(Q, \Delta^k) \neq 0$ , and it is zero otherwise



## Theorem<sup>[1]</sup>

- **Assumption:** Every open subset of  $\mathcal{B}_D$  has positive measure
- **Theorem:** A solution  $Q$ , if it exists, is found in a finite number of steps with probability one
- **Idea of proof:** The distance of  $Q^k$  from the solution set decreases at each correction step

[1] B.T. Polyak and R. Tempo (2001)



## Worst-Case Solution

- The sequential algorithm provides a candidate solution for the set of QMIs
- We can check if this candidate solution satisfies all QMIs and it is a worst-case solution, otherwise we run the algorithm again

- Minimization of a measure of violation for problems that are not strictly feasible<sup>[1,2]</sup>
- Uncertainty in the control matrix,  $B=B(\Delta)$ ,  $\Delta \in \mathcal{B}_D$

We take the feedback law

$$u = YQ^{-1}x$$

where  $Y$  and  $Q=Q^T >0$  are design variables

[1] B.R. Barmish and P. Shcherbakov (1999)

[2] G. Calafiore and B.T. Polyak (2001)



- Related literature on optimization and adaptive control with linear constraints<sup>[1,2,3,4]</sup>
- Stochastic approximation algorithms have been widely studied in the stochastic control and optimization literature<sup>[6,7]</sup>

[1] S. Agmon (1954)

[2] T.S. Motzkin and I.J. Schoenberg (1954)

[3] B.T. Polyak (1964)

[4] V.A. Bondarko and V.A. Yakubovich (1992)

[6] H.J. Kushner and G.G. Yin (2003)

[7] J.C. Spall (2003)

- Design of common Lyapunov functions for switched system<sup>[1]</sup>
- From common to piecewise Lyapunov functions<sup>[2]</sup>
- Ellipsoidal algorithm instead of gradient algorithm<sup>[3]</sup>
- Stopping rule which provides the number of steps<sup>[4]</sup>

[1] D. Liberzon and R. Tempo (2004)

[2] H. Ishii, T. Basar and R. Tempo (2005)

[3] S. Kanev, B. De Schutter and M. Verhaegen (2002)

[4] Y. Oishi and H. Kimura (2003)

- Extensions to optimization problems
- Consider convex function  $f(x)$  and function  $g(x,\Delta)$  convex in  $x$  for fixed  $\Delta$
- Semi-infinite (nonlinear) programming problem

$$\min f(x)$$

$$g(x,\Delta) \leq 0 \text{ for all } \Delta \in \mathcal{B}$$

- Reformulation as stochastic optimization
- **Drawback:** Convergence results are only asymptotic

[1] V. B. Tadic, S. P. Meyn and R. Tempo (2003)

- The scenario approach for convex problems
- Non-sequential method which provides a one-shot solution for general convex problems
- Randomization of  $\Delta \in \mathcal{B}$  and solution of a single convex optimization problem
- Derivation of a new bound on the sample size
- Applications to control systems design

[1] G. Calafiore and M. Campi (2004)

Example<sup>[1]</sup>

- We study a multivariable example for the design of a controller for the lateral motion of an aircraft.
- The model consists of four states and two inputs

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & L_p & L_\beta & L_r \\ \frac{g}{V} & 0 & Y_\beta & -1 \\ N_{\dot{\beta}} \left(\frac{g}{V}\right) & N_p & N_\beta + N_{\dot{\beta}} Y_\beta & N_r - N_{\dot{\beta}} \end{bmatrix} x(t) + \begin{bmatrix} 0 & 0 \\ 0 & -3.91 \\ 0.035 & 0 \\ -2.53 & 0.31 \end{bmatrix} u(t)$$

[1] B.D.O. Anderson and J.B. Moore (1971)



- The state variables are
  - $x_1$  bank angle
  - $x_2$  derivative of bank angle
  - $x_3$  sideslip angle
  - $x_4$  yaw rate
- The control inputs are
  - $u_1$  rudder deflection
  - $u_2$  aileron deflection



## Example - 3

- Nominal values:  $L_p = -2.93$ ,  $L_\beta = -4.75$ ,  $L_r = 0.78$ ,  $g/V = 0.086$ ,  $Y_\beta = -0.11$ ,  $N_\beta = 0.1$ ,  $N_p = -0.042$ ,  $N_\beta = 2.601$ ,  $N_r = -0.29$
- Perturbed matrix  $A(\Delta)$ : each parameter can take values in a range of  $\pm 15\%$  of the nominal value
- Quadratic stability ( $\gamma=0$ ): take  $R=I$  and  $S=0.01I$
- Remark:  $A(\Delta)$  is multiaffine in the uncertain parameters: quadratic stability can be ascertained solving simultaneously  $2^9=512$  LMIs

- Sequential algorithm:
  - Initial point  $Q_0$  randomly selected
  - 800 random matrices  $\Delta^k$
  - The algorithm converged to

$$Q = \begin{bmatrix} 0.7560 & -0.0843 & 0.1645 & 0.7338 \\ -0.0843 & 1.0927 & 0.7020 & 0.4452 \\ 0.1645 & 0.7020 & 0.7798 & 0.7382 \\ 0.7338 & 0.4452 & 0.7382 & 1.2162 \end{bmatrix}$$

- The corresponding controller

$$K = B^T Q^{-1} = \begin{bmatrix} 38.6191 & -4.3731 & 43.1284 & -49.9587 \\ -2.8814 & -10.1758 & 10.2370 & -0.4954 \end{bmatrix}$$

satisfies all the 512 vertex LMIs and therefore it is also a quadratic stabilizing controller in a deterministic sense

- The optimal LQ controller computed on the nominal plant satisfies only 240 vertex LMIs



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# Probabilistic LPV Systems



- **LPV applications:** Aircraft control, automated lane guidance, communication networks
- Parameters  $q=q(t)$  are unknown but bounded in set  $\mathcal{B}_q$
- They can be measured on-line by the controller
- **Critical issue:** Parameter discretization (complexity)

- LPV plant

$$\begin{bmatrix} \dot{x}(t) \\ e(t) \\ y(t) \end{bmatrix} = \begin{bmatrix} A(q(t)) & B_1(q(t)) & B_2(q(t)) \\ C_1(q(t)) & 0 & D_{12}(q(t)) \\ C_2(q(t)) & D_{21}(q(t)) & 0 \end{bmatrix} \begin{bmatrix} x(t) \\ d(t) \\ u(t) \end{bmatrix}$$

with  $q \in \mathcal{B}_q$

- Assumption: Orthogonality conditions are satisfied



- The main goal is to design an LPV controller of the type

$$\begin{bmatrix} \dot{x}_c(t) \\ u(t) \end{bmatrix} = \begin{bmatrix} A_c(q(t)) & B_c(q(t)) \\ C_c(q(t)) & 0 \end{bmatrix} \begin{bmatrix} x_c(t) \\ y(t) \end{bmatrix}$$

such that quadratic performance of the closed-loop system is guaranteed and

$$\sup_d \frac{\left( \int_0^\infty e^T(t) e(t) dt \right)^{\frac{1}{2}}}{\left( \int_0^\infty d^T(t) d(t) dt \right)^{\frac{1}{2}}} < \gamma \quad \forall q \in \mathcal{B}_q$$

## Structured QMI Solution<sup>[1]</sup>

- The LPV problem is solvable if and only if there exist  $X=X^T > 0$  and  $Y=Y^T > 0$  such that for  $\varepsilon > 0$

$$P(X, q) = A(q)X + XA^T(q) + XC_1^T(q)C_1(q)X + \gamma^{-2}B_1(q)B_1^T(q) - B_2(q)B_2^T(q) + \varepsilon I \leq 0$$

$$Q(Y, q) = A^T(q)Y + YA(q) + YB_1(q)B_1^T(q)Y + \gamma^{-2}C_1^T(q)C_1(q) - C_2^T(q)C_2(q) + \varepsilon I \leq 0$$

$$R(X, Y) = - \begin{bmatrix} X & \gamma^{-1}I \\ \gamma^{-1}I & Y \end{bmatrix} \leq 0$$

[1] G. Becker and A. Packard (1994)

- Define a matrix valued function

$$V(X, Y, q) = \begin{bmatrix} P(X, q) & 0 & 0 \\ 0 & Q(Y, q) & 0 \\ 0 & 0 & R(X, Y) \end{bmatrix}$$

and a scalar function

$$v(X, Y, q) = \left\| [V(X, Y, q)]^+ \right\|$$

- **Remark:** The gradients  $\partial_X\{v(X, Y, q)\}$  and  $\partial_Y\{v(X, Y, q)\}$  can be computed in closed form

- We write

$$X^{k+1} = \left[ X^k - \frac{\mu^k \partial_X \{v(X^k, Y^k, q^k)\}}{w(X^k, Y^k, q^k)} \right]^+$$

$$Y^{k+1} = \left[ Y^k - \frac{\mu^k \partial_Y \{v(X^k, Y^k, q^k)\}}{w(X^k, Y^k, q^k)} \right]^+$$

if  $v(X^k, Y^k, q^k) > 0$ , or  $X^{k+1} = X^k$  and  $Y^{k+1} = Y^k$  otherwise

- Here  $\mu^k$  is a stepsize and

$$w(X^k, Y^k, q^k) = \left( \left\| \partial_X \{v(X^k, Y^k, q^k)\} \right\|^2 + \left\| \partial_Y \{v(X^k, Y^k, q^k)\} \right\|^2 \right)^{\frac{1}{2}}$$

- Assume that  $q$  is random vector with support  $\mathcal{B}_q$
- Consider positive measure within  $\mathcal{B}_q$
- **Theorem:** The algorithm converges with probability one in a finite number of iterations
- **Remark:** No assumption on the dependence on  $q$  of matrices  $A, B_1, B_2, C_1, C_2, D_{12}, D_{21}$

[1] Y. Fujisaki, F. Dabbene and R. Tempo (2003)

# RAs for Fault Tolerant Control

- Reformulation of the problem as LPV
- Fault estimate uncertainty  $\delta$  is taken as a random variable with given pdf
- Development of randomized algorithms for computing controller parameters<sup>[1,2]</sup>
- Random generation of  $\delta$  and use of ellipsoidal method

[1] S. Kanev and M. Verhaegen (2004)

[2] S. Kanev (2004)



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# Applications of Randomized Algorithms

- Randomized algorithms have been developed for various specific applications
- Control of **flexible structures**
- Stability and robustness of **high speed networks**
- Stability of **quantized sampled-data** systems
- Brushless **DC motors**
- Control design of **Mini UAV**



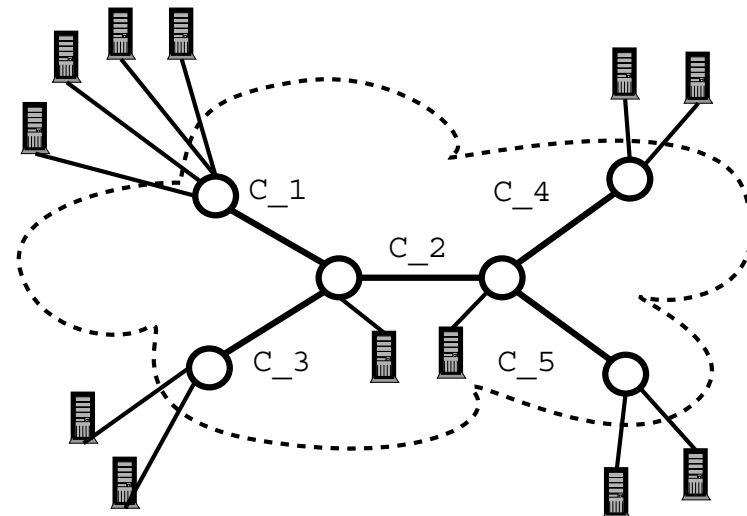
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# Stability and Performance of High-Speed Networks<sup>[1]</sup>

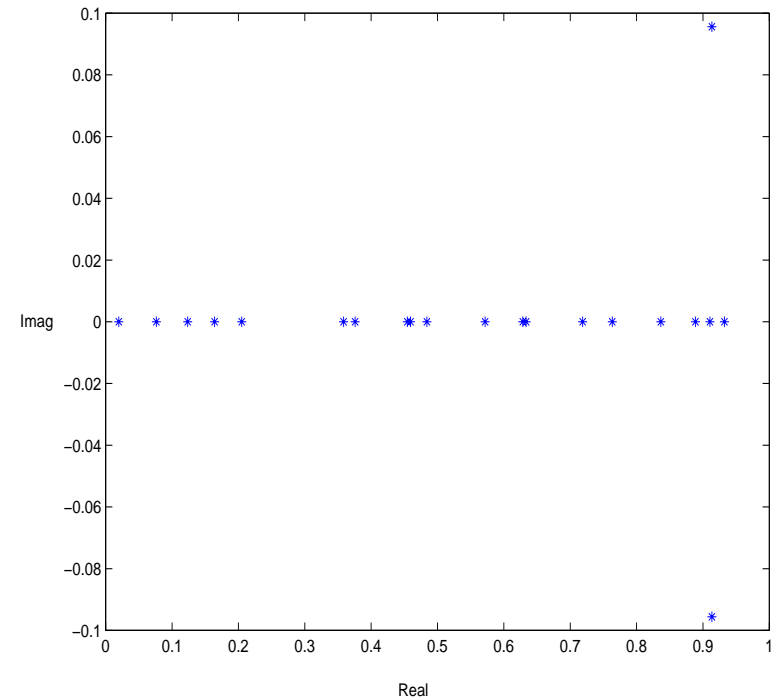
[1] T. Alpcan, T. Basar and R. Tempo (2005)

- Network topology
- Source and destination nodes, links (with buffer and capacity)
- Bottleneck link
- Stability and robustness



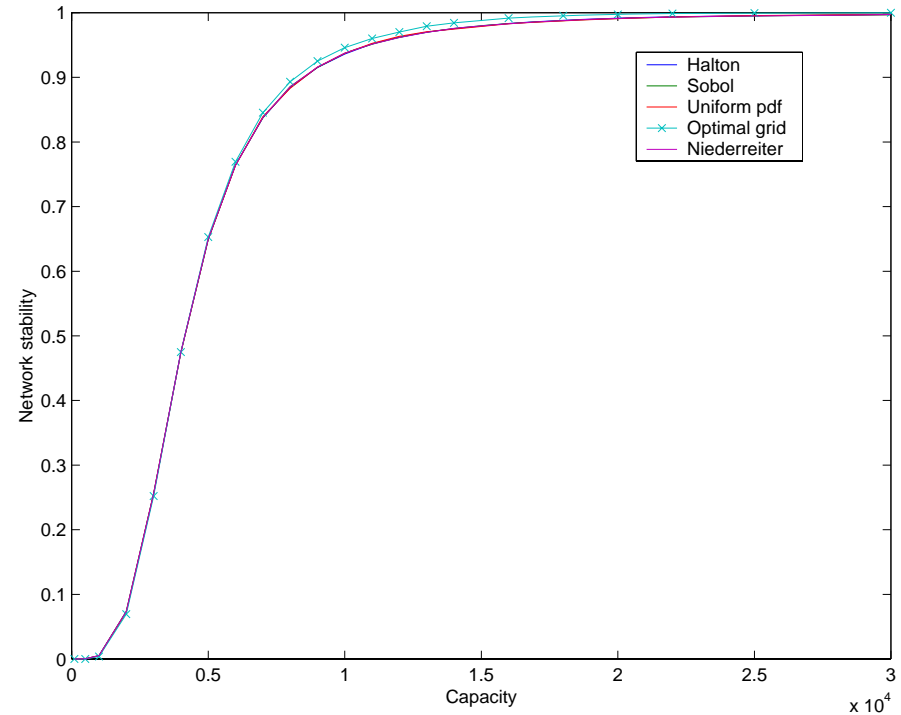
# Symmetric Single Bottleneck

- Parametric stability (discrete time) with real uncertain parameters
- Stability and robustness can be studied in closed form
- Case study with 20 users
- Roots of the closed loop polynomial (discrete-time)



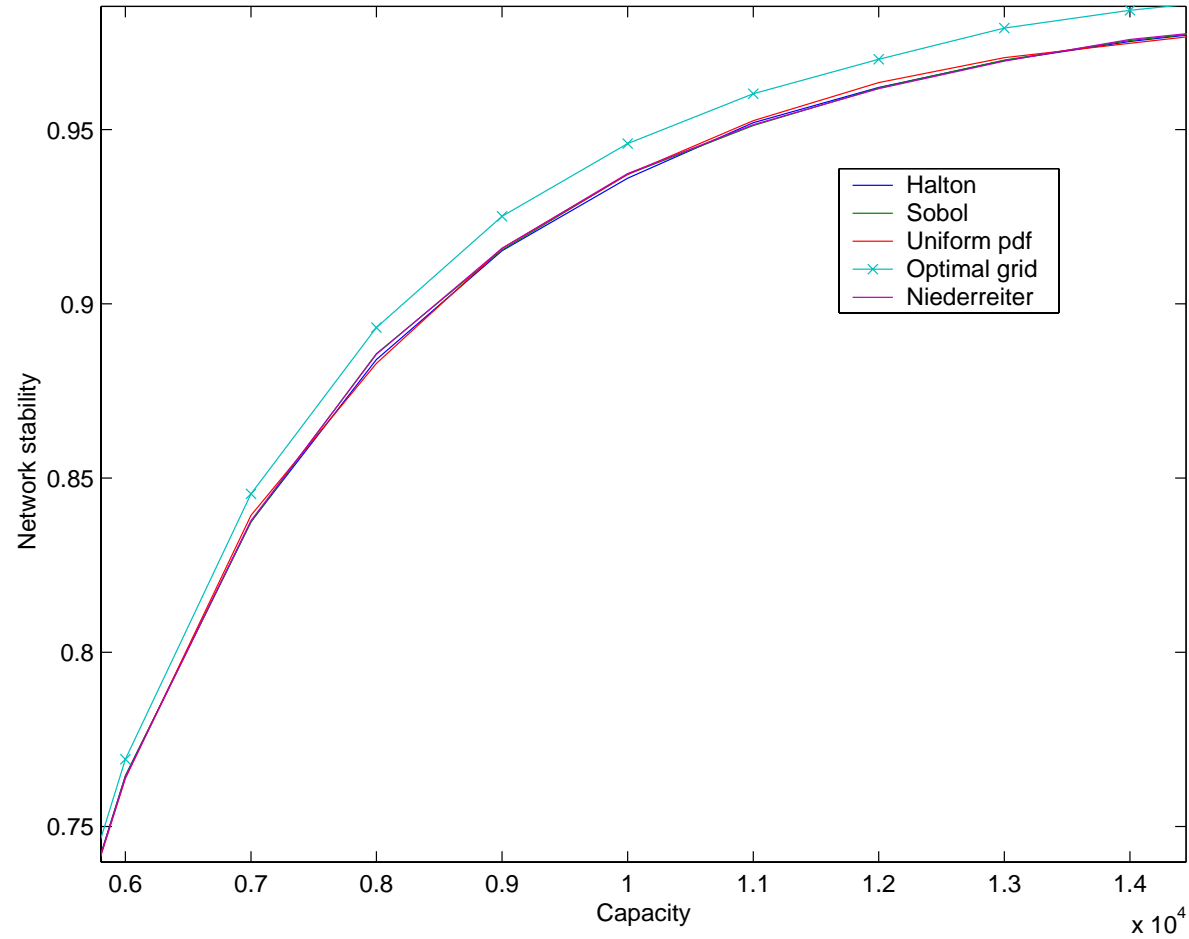
# Non-Symmetric Single Bottleneck

- Closed form analysis is not possible
- We use RAs based on MC and QMC





# Additional Simulations





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# Mini UAV Control Design

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# MH1000: Mini UAV Platform

This activity is supported by the Italian Ministry for Research within the National Project:

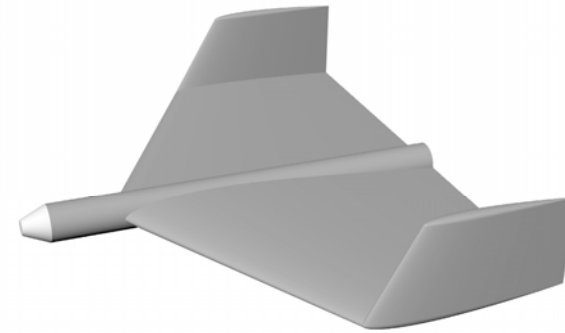
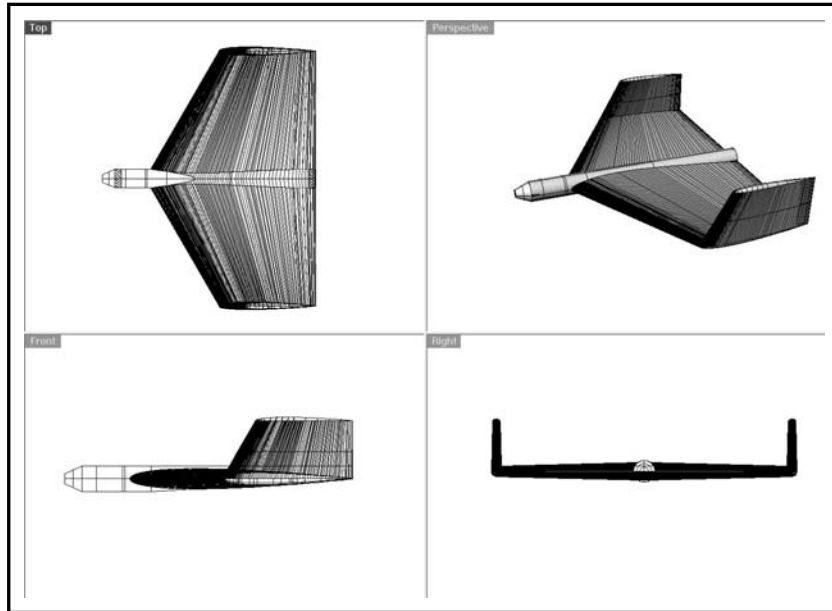
*Study and development of a real-time land control and monitoring system for fire prevention*

The aerial platform is based on the MicroHawk configuration, developed at the Aerospace Engineering Dept. of Politecnico di Torino (national patent no. TO2003A000702, holder Politecnico di Torino, international request PCT/IB2004/002940)



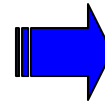
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# MH1000: Mini UAV Platform



## *Design parameter*

wind loading  $W/S = 25 \text{ g/dm}^2$



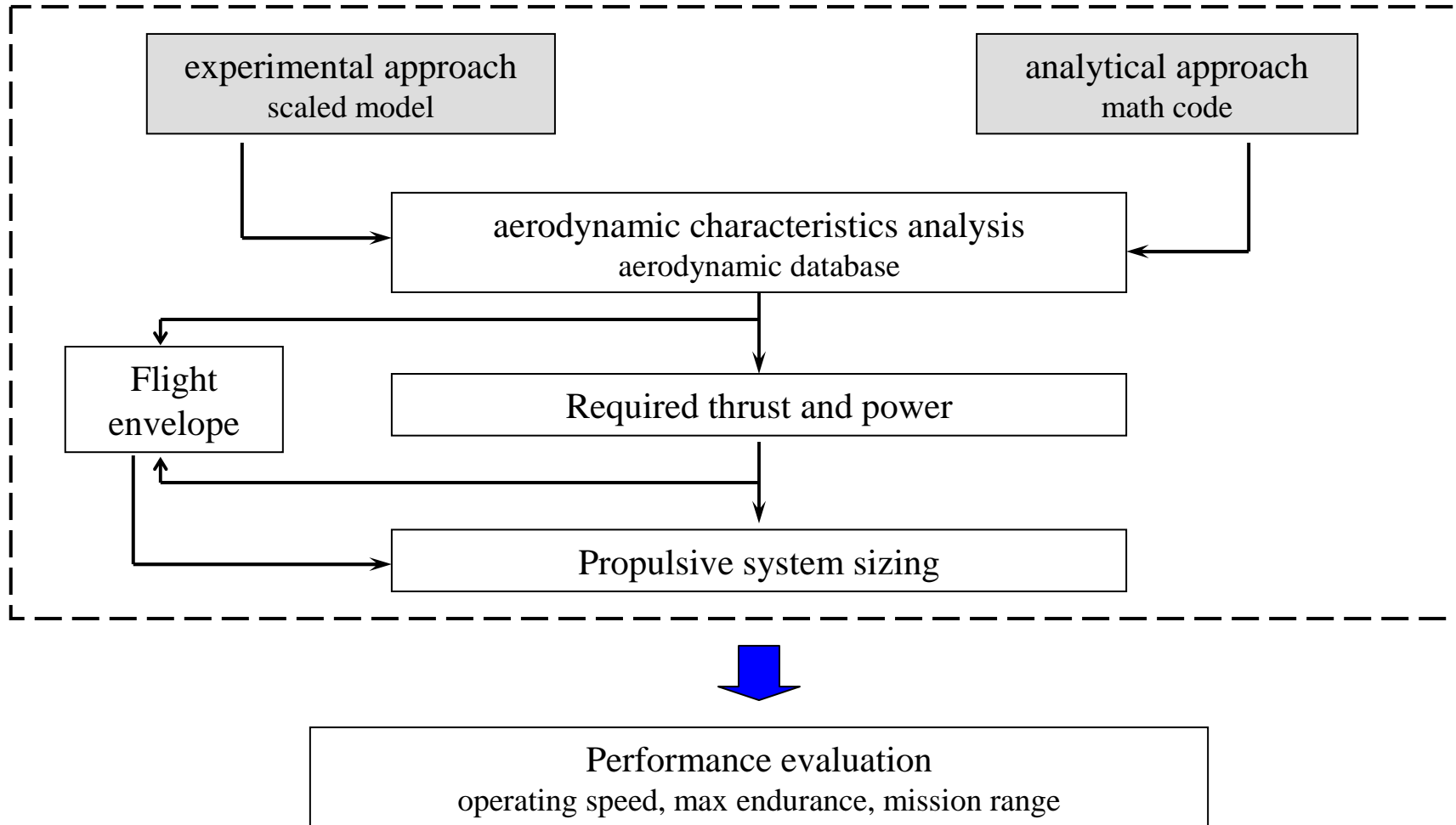
- wingspan 1000 mm
- maximum take-off weight 1500 g
- DC motor
- remote piloting/autonomous flight
- endurance > 30 min



- Aerodynamic and performance analysis
  1. Aerodynamic characteristics
  2. Flight performance
- Basic on-board system
- Weight distribution

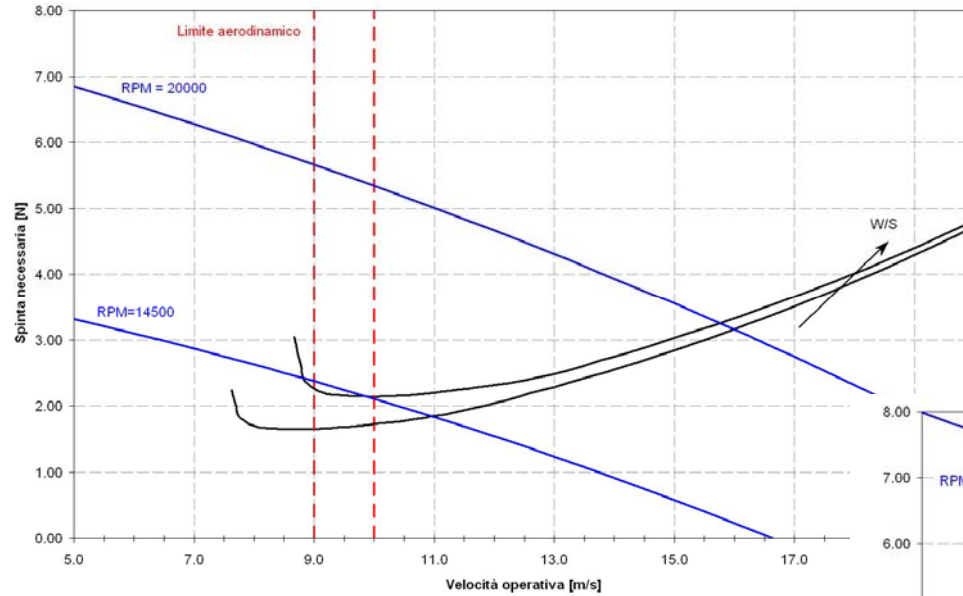


# Aerodynamic/mechanical Analysis





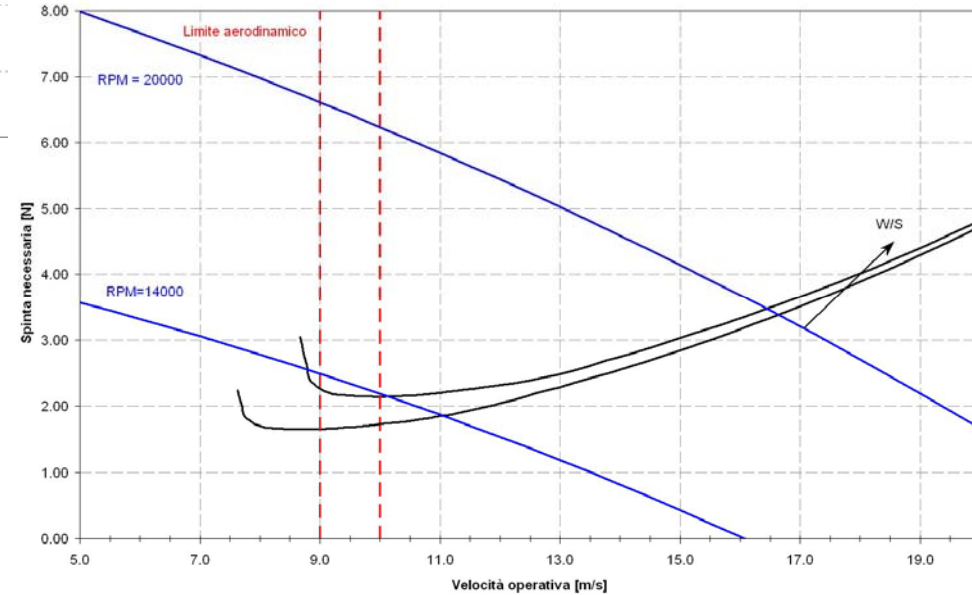
# Flight Envelope



Aerodynamic constraint → minimum flight speed

Propulsive constraint → maximum flight speed

$$V \cong 10 \div 17 \text{ m/s}$$



Wing loading effect → total weight

Propeller sizing effect



# Basic on-board Systems

## DC motor: Hacker B20-15L (4:1)

- weight: 58 g
- dimensions:  $\varnothing$  20 x 40 mm
- Kv: 3700 rpm/volt

## controller: Hacker Master Series 18-B-Flight

- weight: 21 g
- dimensions: 33 X 23 X 7 mm
- current drain: 18 A

## battery: Kokam 2000HD (3x)

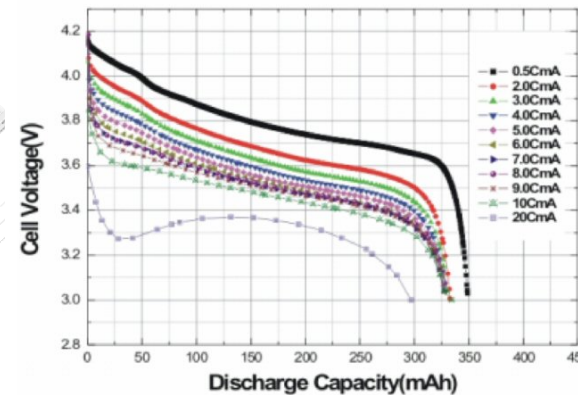
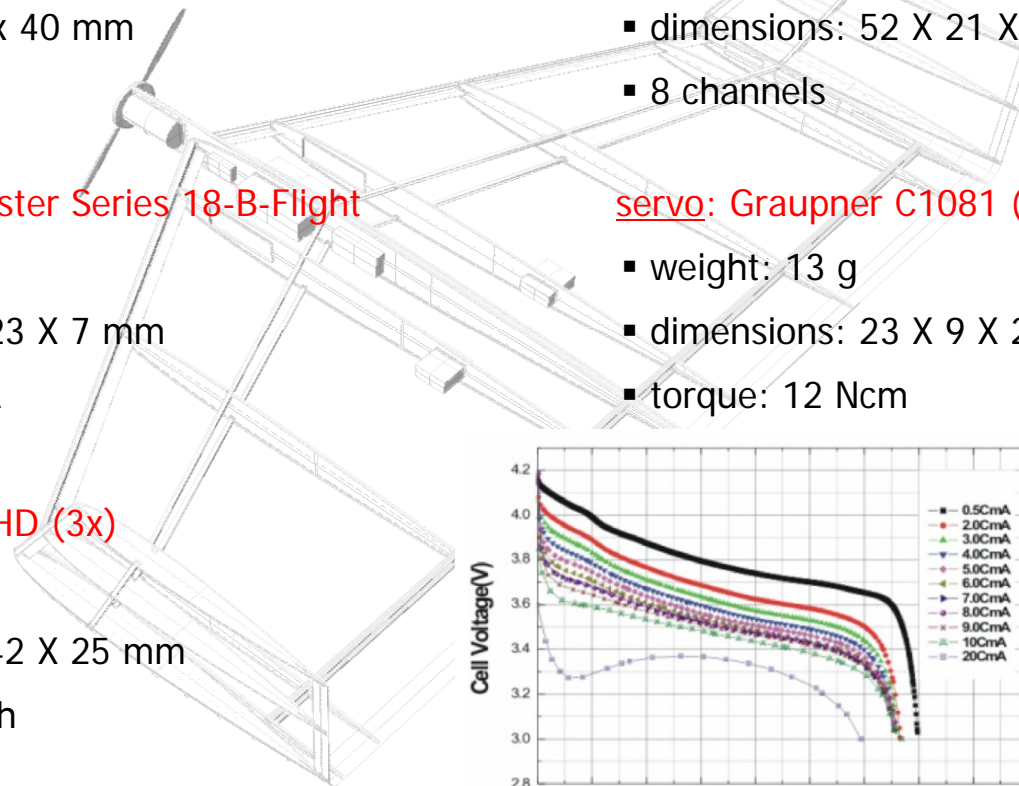
- weight: 160 g
- dimensions: 79 X 42 X 25 mm
- capacity: 2000 mAh

## receiver: Schulze Alpha840W

- weight: 13.5 g
- dimensions: 52 X 21 X 13 mm
- 8 channels

## servo: Graupner C1081 (2x)

- weight: 13 g
- dimensions: 23 X 9 X 21 mm
- torque: 12 Ncm



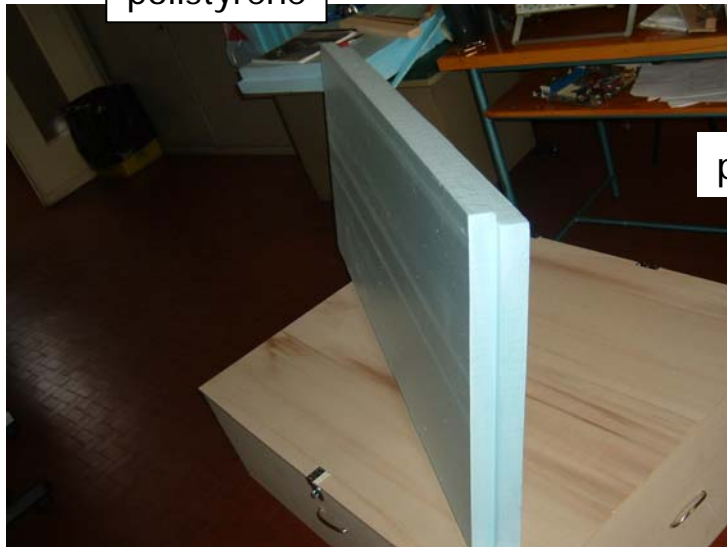


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# Prototype Manufacturing - 1

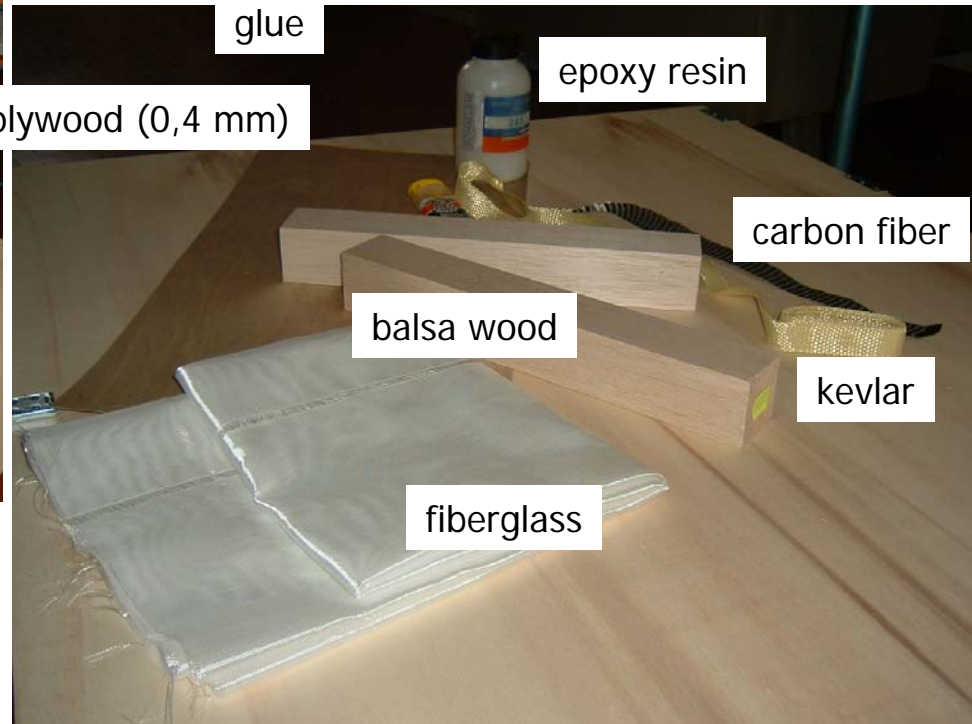
material

polistyrene



glue

plywood (0,4 mm)



epoxy resin

carbon fiber

balsa wood

kevlar

fiberglass



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# Prototype Manufacturing - 2



hot wire foam cutting machine



working instruments

lifting surfaces outline



slide outline



fuselage reference



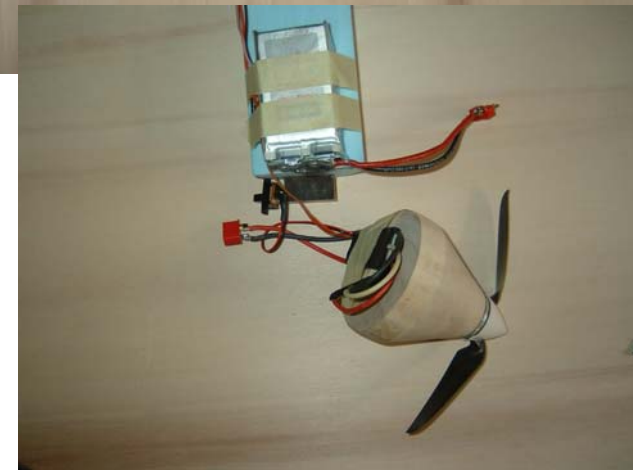
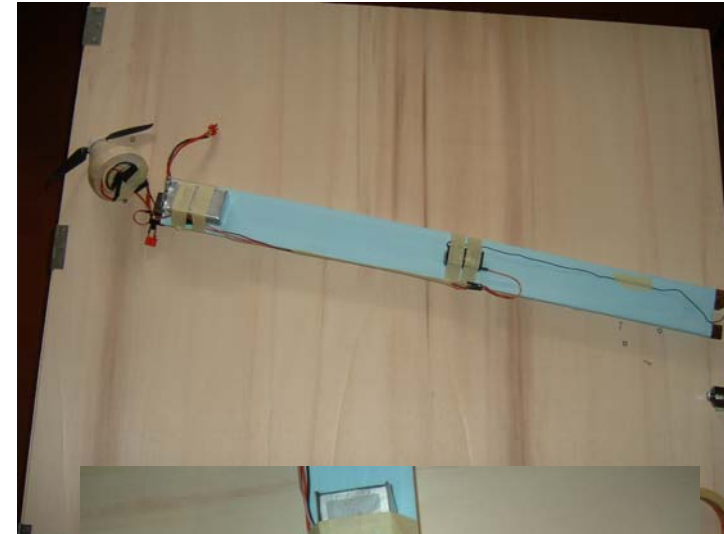
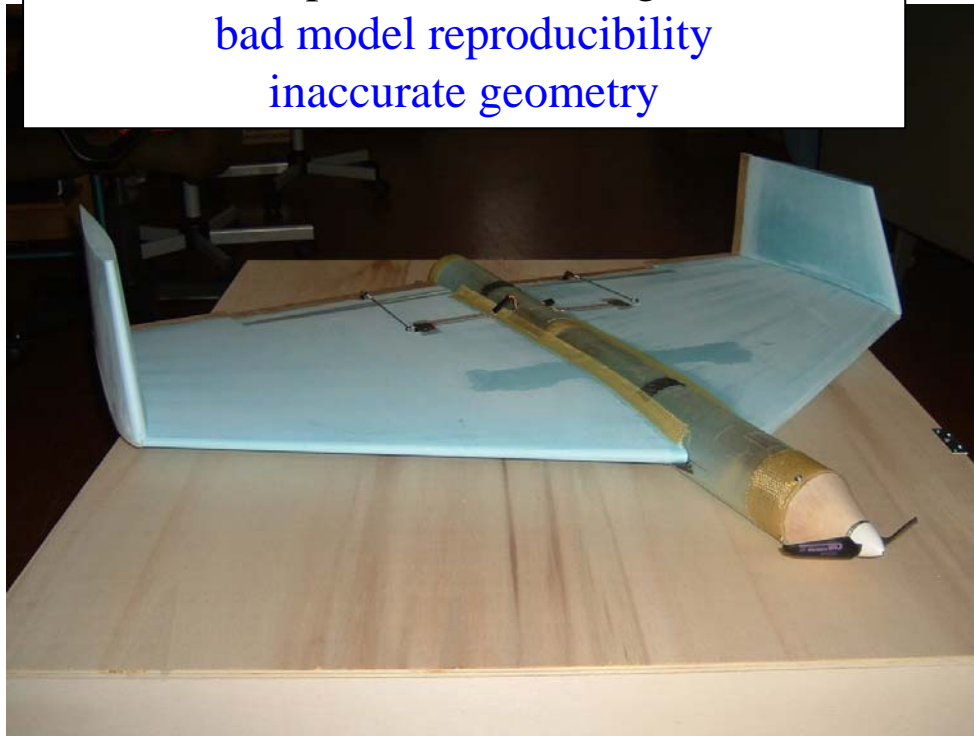


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# Prototype Manufacturing - 3

prototype

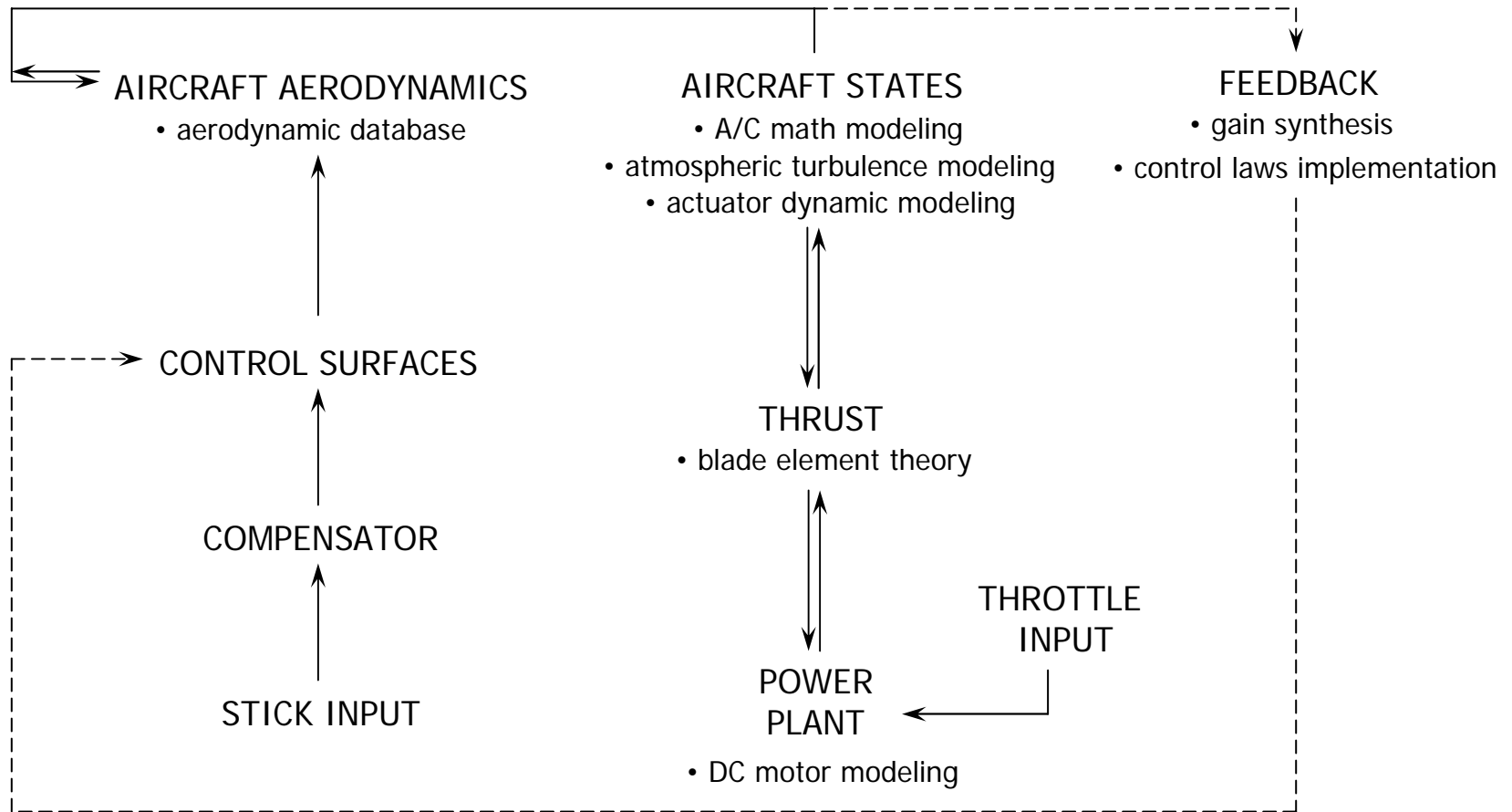
easy construction  
rapid manufacturing  
bad model reproducibility  
inaccurate geometry





# Aircraft Dynamics - 1

Aircraft math model implementation within an off-line flight simulator

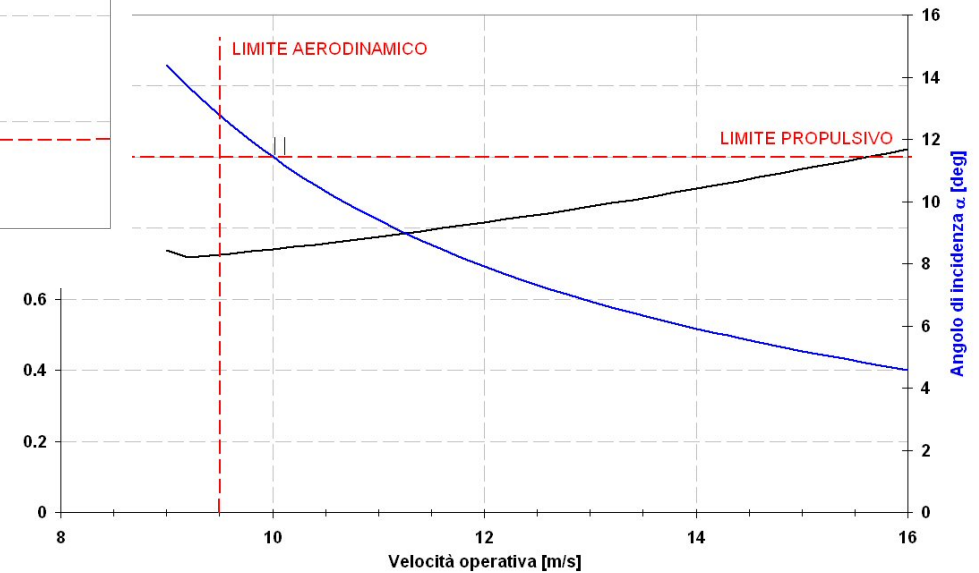
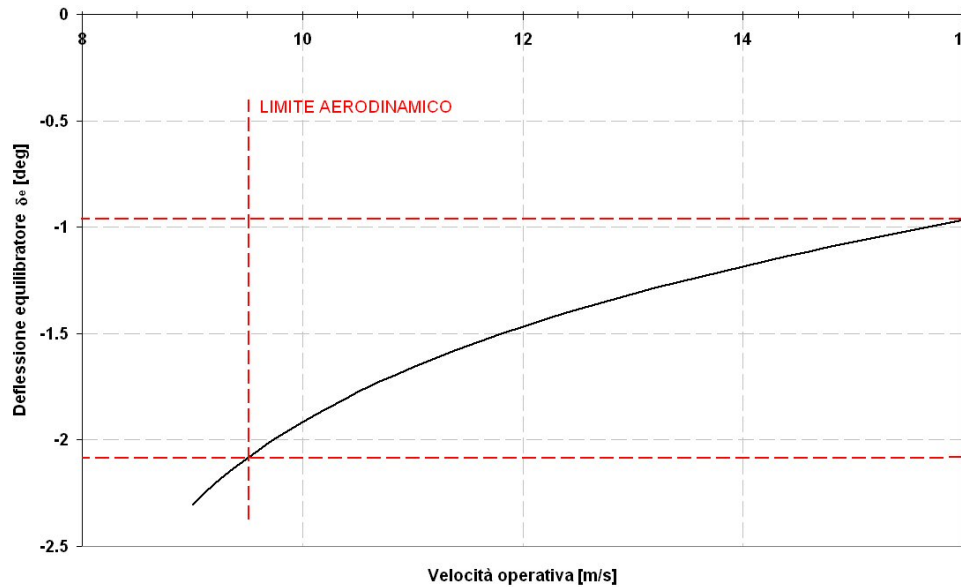




# Aircraft Dynamics - 2

Aircraft math model implementation within an off-line flight simulator

➤ trimmability analysis



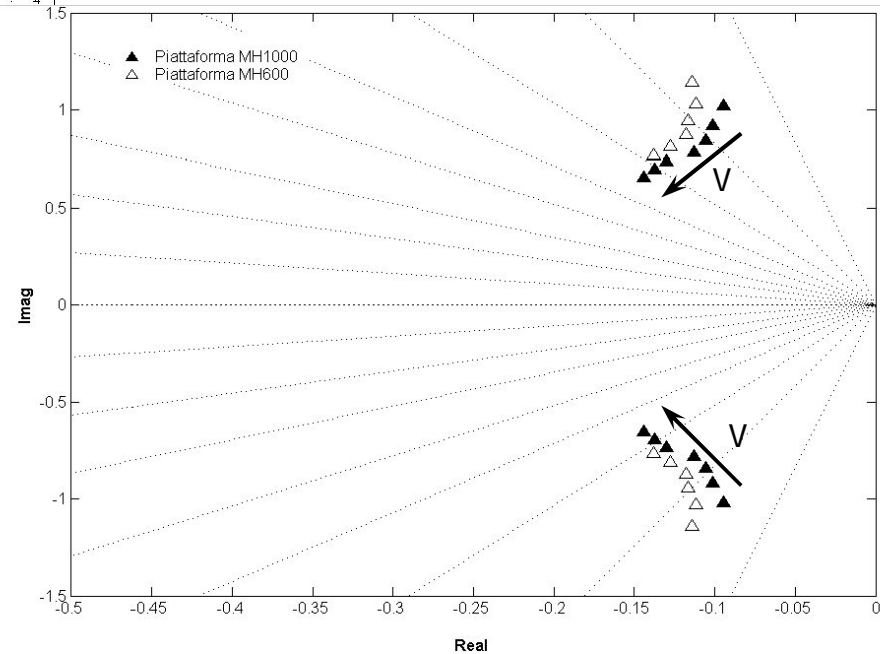
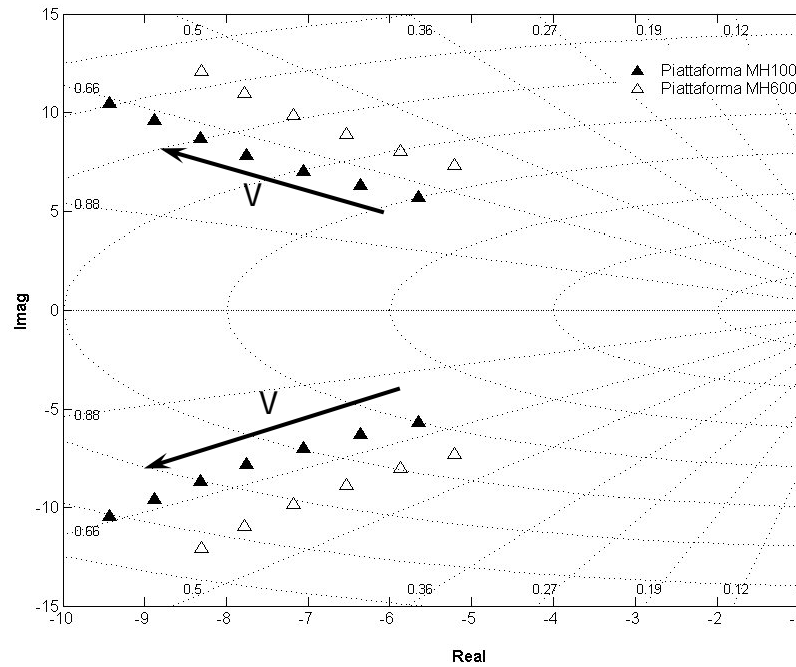


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# Aircraft Dynamics - 3

Aircraft math model implementation within an off-line flight simulator

➤ *open loop* dynamics characterization

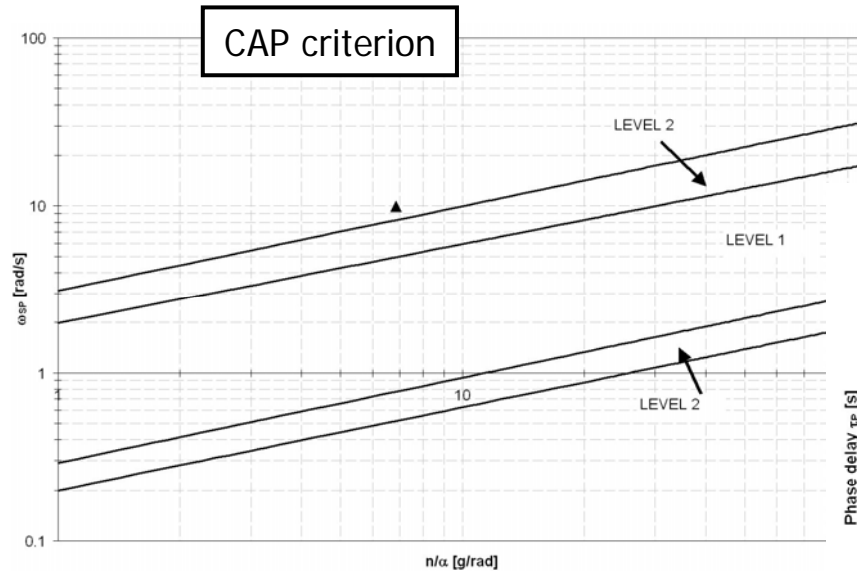




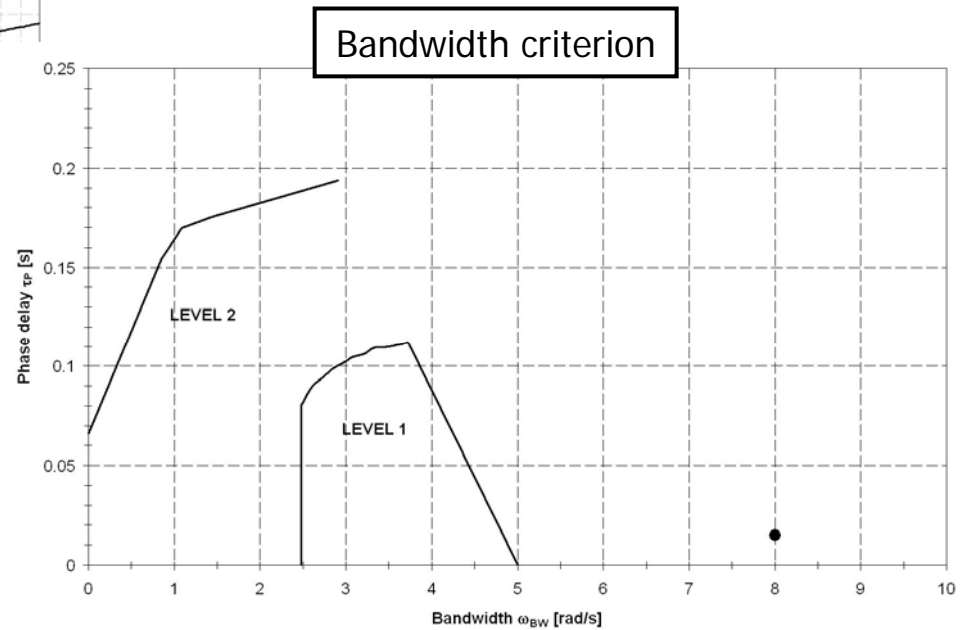
# Aircraft Dynamics - 4

Aircraft math model implementation within an off-line flight simulator

➤ compliance to standard requirements



MIL 8785C/MIL 1797A standards

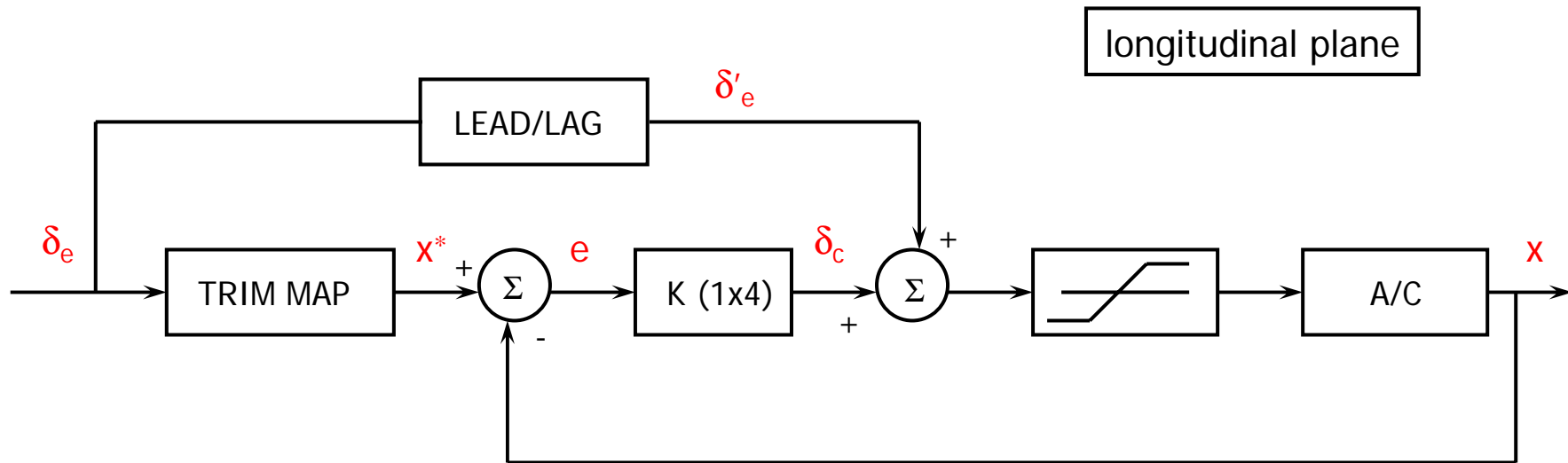




# Controller Design - 1

## Flight control system for platform stabilization

➤ definition of controller architecture



$$X \equiv \text{state vector} = \{u \quad \alpha \quad q \quad \theta\}$$



# Controller Design - 2

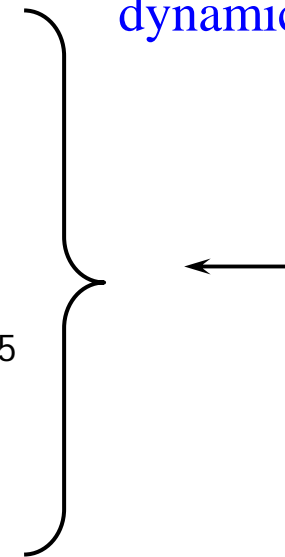
Flight control system for platform stabilization

Gain synthesis

- Randomized algorithms
- Enlarged stability concept – bounds
  - ✓ stable eigenvalues  $\rightarrow \text{Re}(\lambda) < 0$
  - ✓ complex conjugate eigenvalues  $\rightarrow \text{Im}(\lambda) \neq 0$
  - ✓ short period undamped frequency  $\rightarrow 4 < \omega_{sp} < 6$
  - ✓ short period damping  $\rightarrow 0.5 < \zeta_{sp} < 0.9$
  - ✓ phugoid mode undamped frequency  $\rightarrow 1 < \omega_{ph} < 1.5$
  - ✓ phugoid mode damping  $\rightarrow 0.1 < \zeta_{ph} < 0.15$
  - ✓  $\Delta\omega < \pm 15\% \omega_{min}, \omega_{max}$

standard requirements

dynamics analysis





# Controller Design - 3

Flight control system for platform stabilization

*stability robustness analysis*

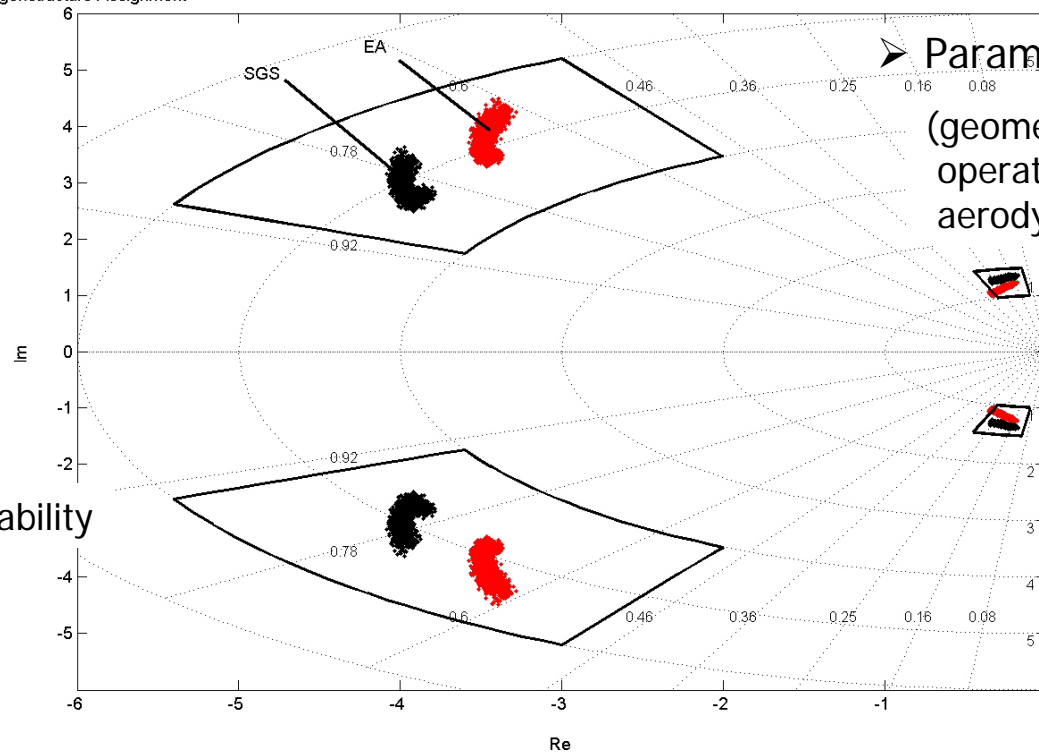
➤ Randomized algorithms

SGS | Stochastic Gain Synthesis  
EA | Eigenstructure Assignment

➤ Parameter uncertainties

(geometric and inertial data  
operating conditions  
aerodynamic database)

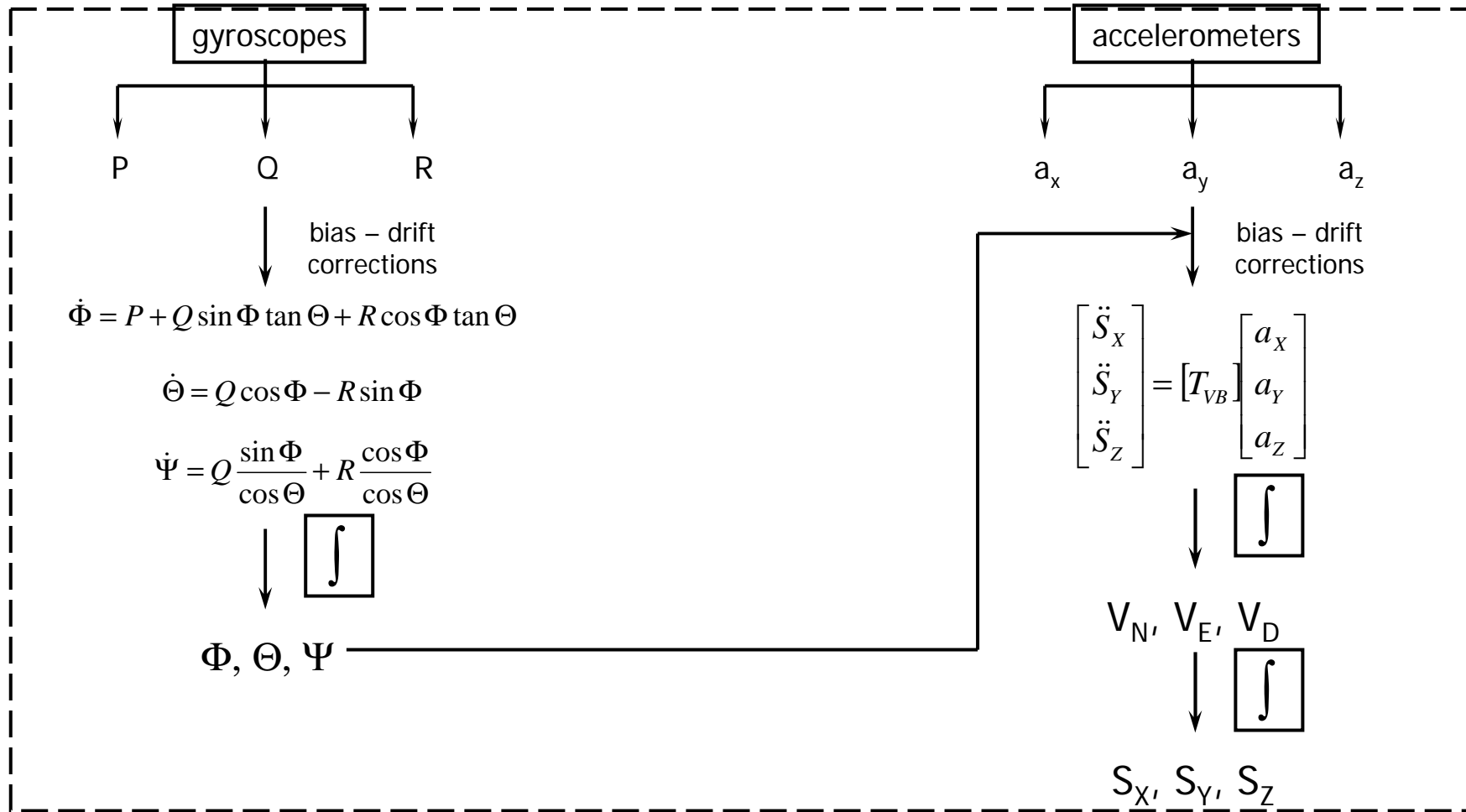
Probability of instability





# Controller Design - 4

## Autopilot

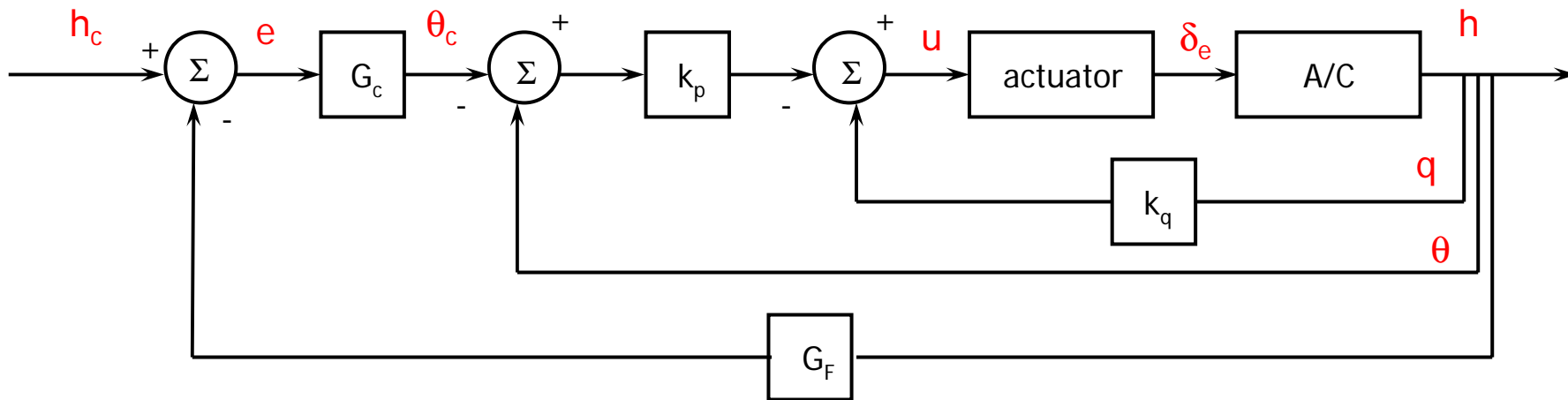




# Controller Design - 5

Autopilot

altitude hold





# Flight Simulator



Implementation of the platform mathematical model within a real-time flight simulator

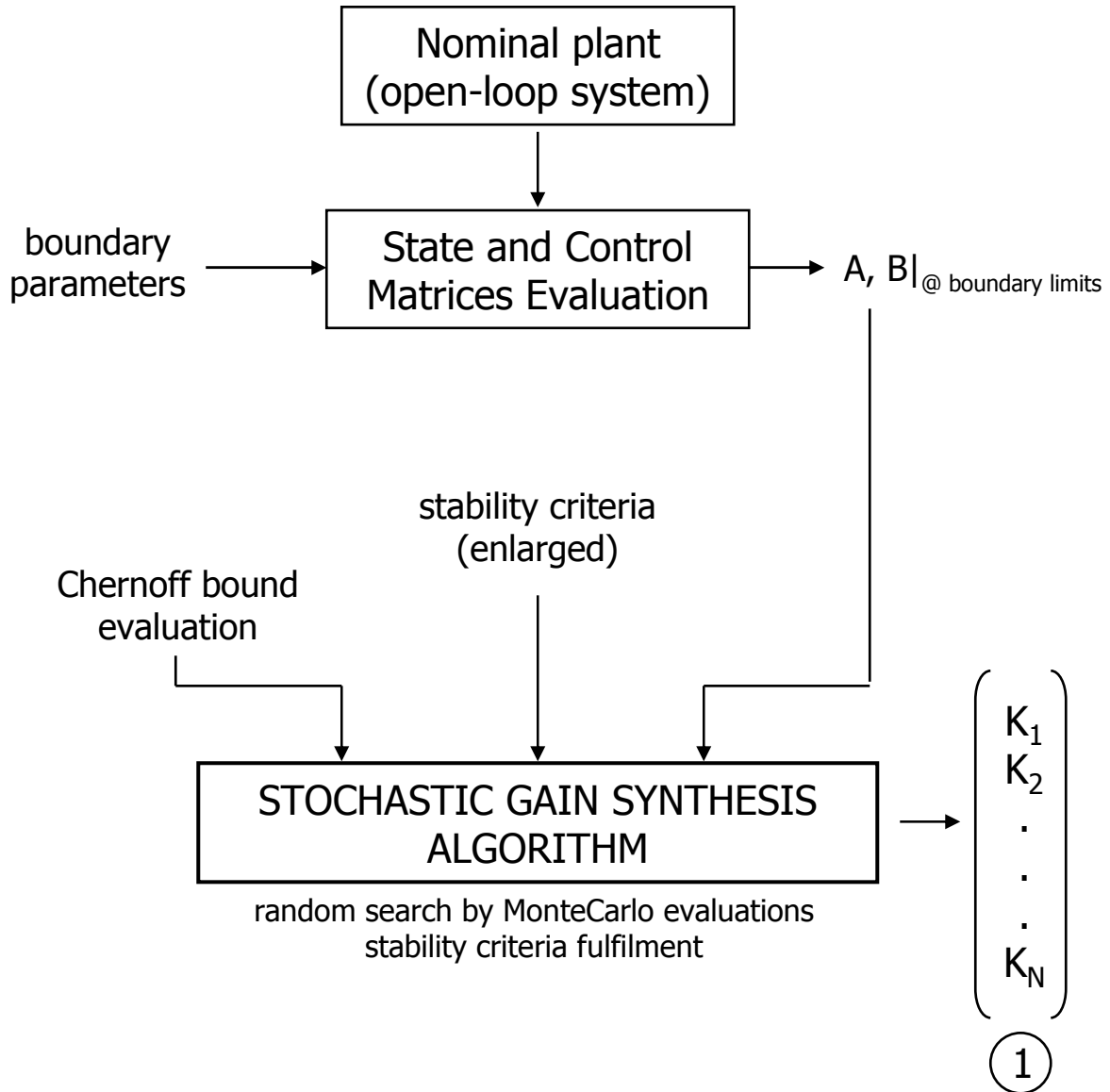
Remote piloting by means of joystick and RC transmitter



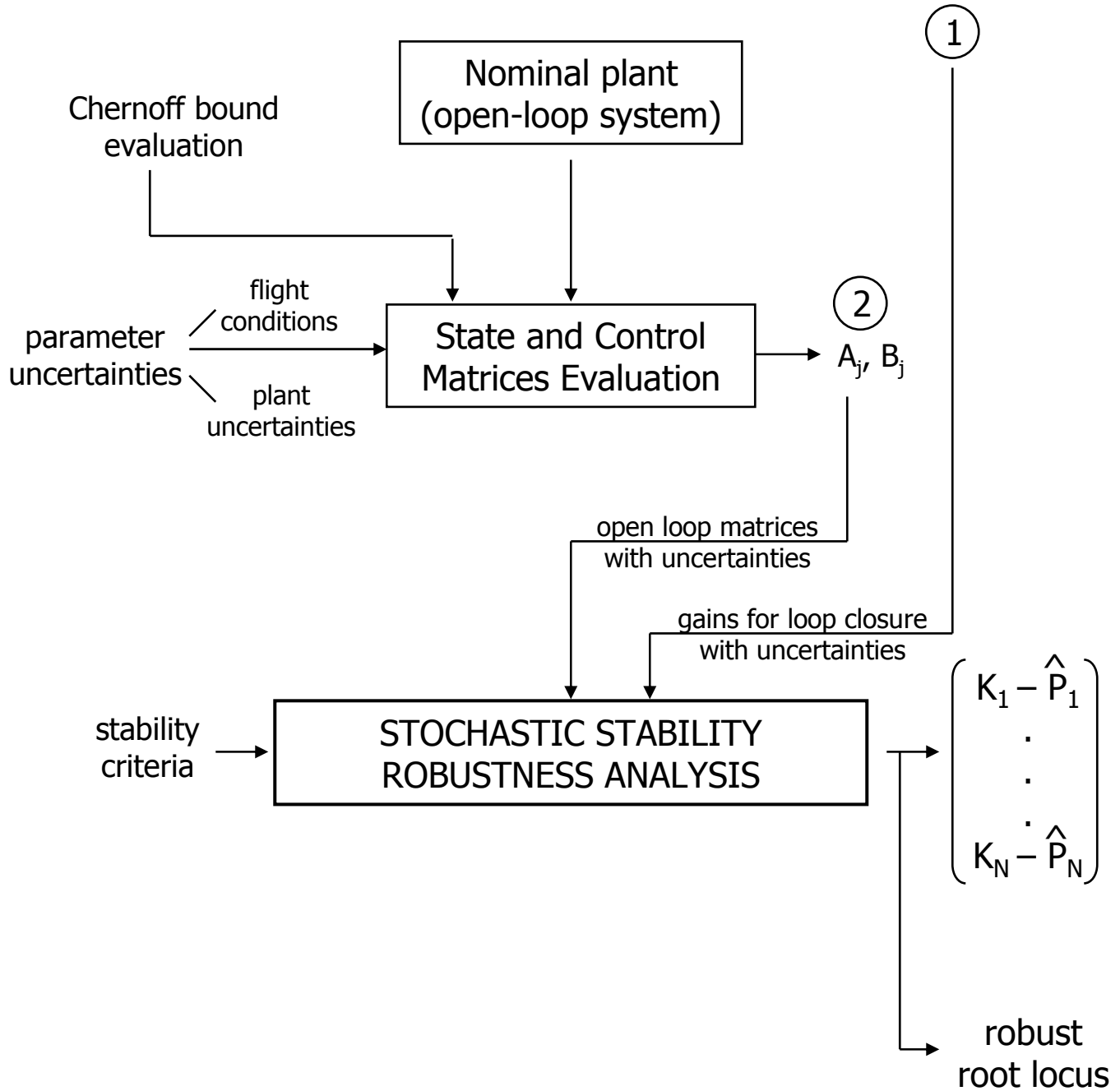


- Three main phases
  1. Synthesis
  2. Stability Analysis
  3. Performance Analysis
  
- Numerical computation of A, B matrices
- User defined specs
- State feedback control
- Randomized algorithms

## Phase 1: Synthesis



## Phase 2: Stability Analysis



## Phase 3: Performance Analysis

